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1 **Acute effects of different orthoses on lower extremity kinetics and kinematics during**
2 **running: a musculoskeletal simulation analysis.**

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8 **Keywords:** Running, orthoses, biomechanics, pathology.

9 **Abstract**

10 PURPOSE: The current investigation aimed to examine the effects of different orthotic
11 conditions on the biomechanical mechanisms linked to the aetiology of chronic pathologies
12 using musculoskeletal simulation. METHODS: 16 male and 20 females ran over an
13 embedded force plate at 4.0 m/s, in five different conditions (medial, lateral, no-orthoses,
14 semi-custom and off the shelf). Kinematics of the lower extremities were collected using an
15 eight-camera motion capture system and lower extremity joint loading also explored using a
16 musculoskeletal simulation approach. Differences between orthoses conditions were
17 examined using 2 x 2 mixed ANOVA. RESULTS: **External instantaneous** load rate was
18 significantly reduced in the off the shelf orthoses (male=1290.60 and female=1567.10N/kg/s)
19 compared to the medial (male=1480.45 and female = 1767.05N/kg/s) and semi-custom
20 (male=1552.99 and female=1704.37N/kg/s) conditions. In addition, peak patellofemoral
21 stress was significantly lower in the **off the shelf** orthoses (male=68.55 and
22 female=94.91KPa/kg) compared to the lateral condition (male=70.49 and
23 female=103.22KPa/kg). Finally, peak eversion angles were significantly attenuated in the

24 medial orthoses (male=-6.61 and female=-7.72deg) compared to the lateral (male=-9.61 and
25 female=-10.32deg), no-orthoses (male=-8.22 and female=-10.10deg), semi-custom (male=-
26 8.25 and female=-9.49deg) and off the shelf (male=-7.54 and female=-8.85deg) conditions.
27 CONCLUSIONS: The current investigation shows that different orthotic devices/
28 configurations may provide distinct benefits in terms of their effectiveness in attenuating the
29 biomechanical parameters linked to the aetiology of chronic running injuries.

30

31 **Introduction**

32 Regular engagement with distance running has long been associated with a plethora of
33 physiological and psychological advantages. However, due to its cyclical nature, distance
34 running is also associated with an extremely high incidence of chronic pathologies; **with an**
35 **occurrence rate of up to 70 % (Taunton et al., 2002).** Specifically, patellofemoral pain, tibial
36 stress fractures, medial tibial stress syndrome, Achilles tendinopathy and pain secondary to
37 hip and knee osteoarthritis are common complaints reported by runners (Taunton et al., 2002,
38 Van Ginckel et al., 2009; **Lopes et al., 2012**; Snyder et al., 2006).

39

40 Patellofemoral pain is the most common chronic pathology in runners (Taunton et al., 2002).
41 Elevated patellofemoral joint stress is the biomechanical parameter most strongly linked to
42 the aetiology of patellofemoral pain syndrome (Farrokhi et al., 2011). Patellofemoral pain
43 symptoms persist for many years, and importantly >45% of individuals with patellofemoral
44 pain later present with osteoarthritis at this joint (**Hinman et al., 2014**). In addition,
45 degenerative tibiofemoral joint pathologies account for up to 16.8% of knee pathologies in
46 runners (Taunton et al., 2002). The medial tibiofemoral compartment is considered

47 significantly more prone to degeneration than the lateral aspect (Wise et al., 2012), and the
48 biomechanical parameter most strongly associated with the initiation of knee osteoarthritis is
49 the magnitude of the compressive load experienced at the joint (Morgenroth et al., 2014).

50

51 Furthermore, Achilles tendinopathy is also a common chronic pathology in runners,
52 responsible for up to 15% of all reported injuries (Van Ginckel et al., 2009). Although
53 regarded as the strongest tendon in the body, the Achilles tendon is subjected to forces up to 7
54 * bodyweight during running (Almondroeder et al., 2013). Excessive cyclic stresses borne the
55 tendon are regarded as the main biomechanical stimulus for the initiation of Achilles
56 tendinopathy (Abate et al., 2009). Additionally, medial tibial stress syndrome is similarly a
57 frequently reported chronic running injury cause of running-related injury, accounting for
58 $\geq 13.6\%$ of all injuries and causing discomfort at the postero-medial aspect of the tibia
59 (Lopes et al., 2012). The biomechanical mechanisms most prominently linked to the
60 aetiology of medial tibial stress syndrome are the magnitudes of plantarflexion range of
61 motion and hip external rotation range of motion (Hamstra-Wright et al., 2015). Finally, tibial
62 stress fractures are also a serious chronic musculoskeletal injury in runners, representing
63 between 0.5-21.1% of all pathologies (Snyder et al., 2006). The distal-anterior aspect of the
64 tibia is the most frequent location for stress fractures, and retrospective analyses indicate that
65 excessive tibial accelerations/ vertical rates of loading are the biomechanical mechanisms
66 predominantly responsible for the development of stress fractures (Warden et al., 2006).

67

68 Taking into account the rate of chronic pathologies in runners, conservative prophylactic
69 strategies are a key priority for clinical analyses. Foot orthoses are commonly utilized for the
70 prevention/ treatment of chronic running injuries, and a range of foot orthoses are available,

71 typically classified either as off-the-shelf or custom devices. Off-the-shelf devices are
72 prefabricated by the manufacturer and the design/ fit of the devices are predetermined.
73 Custom orthoses conversely allow the shape, design and fit of the orthotic to be specifically
74 tailored to the individual. However, custom orthoses are typically very expensive and can
75 take several weeks to manufacture. Therefore, orthotic manufacturers have introduced semi-
76 custom devices which can be heat moulded to fit each runner's feet more readily, but at a
77 much lower cost in relation to fully customized devices. In addition to traditional foot
78 orthoses, wedged orthoses that are built up along either the medial or lateral edges have also
79 become common in recent years (Aminian et al., 2014). Wedged devices focus more
80 specifically on modifying the alignment of the lower extremities rather than providing
81 cushioning (Sinclair et al., 2019). Previous clinical analyses have shown that orthoses may be
82 effective in reducing the incidence of lower limb injuries. Bonanno et al., (2018) showed that
83 prefabricated foot orthoses mediated a 34% reduction in the risk of developing medial tibial
84 stress syndrome, patellofemoral pain, Achilles tendinopathy or plantar fasciitis in Australian
85 navy recruits. Similarly, Franklyn-Miller et al., (2011) showed that military officer trainees
86 who received custom orthoses had a significantly reduced absolute injury risk (1 injury per
87 4666 hours of training) compared to a control group (1 injury per 1600 hours of training).
88 Finally, Sinclair et al., (2018) showed that semi-custom foot orthoses mediated significant
89 reductions patellofemoral pain symptoms in runners from both the strong and weak & tight
90 subgroups of patellofemoral pain patients.

91

92 The effects of foot orthoses on lower extremity kinetics and kinematics during running has
93 been explored previously in biomechanical literature. Laughton et al., (2003) and
94 Mündermann et al., (2003) found that off the shelf orthoses significantly reduced tibial
95 accelerations and loading rates during running, although Butler et al., (2003) showed that

96 custom devices had no effect on impact loading parameters. Sinclair et al., (2017) showed
97 that medial orthoses reduced peak eversion and tibial internal rotation, yet Almonroeder et
98 al., (2016) showed using off the shelf devices that eversion/ tibial internal rotation parameters
99 were not significantly affected. In addition, Sinclair et al., (2014) also showed that off the
100 shelf orthoses significantly reduced peak Achilles tendon force, but Sinclair et al., (2015)
101 revealed that semi-custom orthoses had no effect on Achilles tendon kinetics in female
102 runners. Finally, Sinclair, (2018) showed that both medial and lateral orthoses significantly
103 increased patellofemoral kinetics during the stance phase. Foot orthoses are utilized as
104 blanket term for a range of distinct devices that may include off the shelf, custom orthoses,
105 semi-custom devices, heel-lifts, lateral/medial wedges and flat insoles. To date there has yet
106 to be a published investigation of the biomechanical effects of off the shelf, semi-custom, and
107 medial/ lateral orthoses on lower extremity kinetics and kinematics linked to the aetiology of
108 chronic running injuries.

109

110 In addition, previous analyses examining the biomechanical effects of foot orthoses, have
111 utilized joint torque driven musculoskeletal modelling approaches to quantify the loads
112 experienced by the lower extremities. However, as skeletal muscle forces are the main
113 contributors to lower extremity joint loading; musculoskeletal modelling methodologies may
114 not necessarily characterize localized joint kinetics (Herzog et al., 2003). Therefore, more
115 contemporary musculoskeletal simulation based approaches, which allow skeletal muscle
116 forces to be simulated during human movement, and employed as inputs to calculate lower
117 extremity joint reaction forces may be more appropriate (Delp et al., 2007). Such approaches
118 have not yet been adopted to explore biomechanical differences between different orthoses
119 during running.

120

121 Therefore, the aim of the current investigation was to examine the effects of the
122 aforementioned orthotic conditions on the biomechanical mechanisms linked to the aetiology
123 of chronic pathologies, using a musculoskeletal simulation based analysis. An investigation
124 of this nature may provide insight into the potential efficacy of different foot orthoses for the
125 prevention chronic running pathologies.

126

127 **Methods**

128 *Participants*

129 Thirty-six participants (16 male and 20 female) volunteered to take part in the current
130 investigation. The mean and standard deviation characteristics of the participants were (male:
131 age 28.69 ± 6.06 years, height 177.75 ± 5.02 cm, body mass 76.58 ± 8.68 kg and foot posture
132 index = 3.00 ± 1.63 and female: age 32.25 ± 7.36 years, height 161.29 ± 5.61 cm, body mass
133 65.51 ± 7.34 kg and and foot posture index = 3.90 ± 2.43). All identified as recreational
134 runners who trained 3 times/week, completing a minimum of 35 km. Participants were all
135 injury free at the time of data collection and had not undergone lower extremity
136 musculoskeletal surgery. The procedure utilized for this investigation was approved by the
137 University of Central Lancashire, Science, Technology, Engineering and Mathematics,
138 ethical committee (Ref: 874) and all participants provided written informed consent.

139

140 *Orthoses*

141 Five experimental conditions were examined in this investigation (lateral, medial, semi-
142 custom, off the shelf and no orthotic). For the medial and lateral orthoses, commercially
143 available full-length orthoses (Slimflex Simple, High Density, Full Length, Algeos UK) were
144 examined. The orthoses were able to be modified to either a 5° varus or valgus configuration
145 which in two separate components spanning the full length of the device. The orthoses were
146 made from ethylene-vinyl acetate with a shore A rating of 65 and had a heel thickness of 11
147 mm including the additional wedge. The semi-custom insoles (Sole Control, Sole, Milton
148 Keynes, UK), were made from ethylene-vinyl acetate with a shore A 30 hardness rating and a
149 heel thickness of 6 mm. To mould the insoles, they were placed into a pre-heated oven (90
150 °C) for a duration of two minutes. The heated insoles were then placed inside the shoes and
151 participants were asked to stand upright without moving for two minutes to allow the process
152 of moulding the insoles to the longitudinal arch profile of each participant, in accordance
153 with manufacturer instructions. The off the shelf orthoses (Sorbothane, shock stopper sorbo
154 Pro, Nottinghamshire, UK) were made from a custom polyurethane polymer and had a heel
155 thickness of 6 mm and a shore A hardness rating of 10. To ensure consistency each
156 participant wore the same footwear (Asics, Patriot 6). The experimental footwear had a mean
157 mass of 0.265 kg, heel thickness of 22 mm and heel drop of 10 mm. The order that
158 participants ran in each orthotic condition was counterbalanced.

159

160 *Procedure*

161 Participants ran across a 20 m biomechanics laboratory surface (MondoSport Ramflex,
162 Mondo, Italy) at 4.0 m/s ($\pm 5\%$), striking an embedded piezoelectric force platform (Kistler,
163 Kistler Instruments Ltd., Alton, Hampshire), which sampled at 1000 Hz, with their right
164 (dominant) foot. Running velocity was monitored using infrared timing gates (Newtest, Oy

165 Koulukatu, Finland). The stance phase was delineated as the duration over which 20 N or
166 greater of vertical force was applied to the force platform. Runners completed five successful
167 trials in each of the five different orthotic conditions. A successful trial was defined as one
168 within the specified velocity range, where all tracking clusters were in view of the cameras,
169 the foot made full contact with the force plate and there was no evidence of gait
170 modifications due to the experimental conditions. The order that participants ran in each
171 condition was counterbalanced, by providing each orthotic with a letter from A-E and block
172 counterbalancing the order in which each was presented to each participant. Kinematics and
173 ground reaction forces data were synchronously collected. Kinematic data was captured at
174 250 Hz via an eight-camera motion analysis system (Qualisys Medical AB, Goteburg,
175 Sweden). Dynamic calibration of the motion capture system was performed before each data
176 collection session.

177

178 After being tested in each orthotic condition, participants were asked to provide their rating
179 of the comfort of each one. The comfort measurement procedure consisted of a 150 mm
180 visual analogue scale with the extreme left side being indicative of ‘not comfortable at all’
181 and the extreme right of the scale labelled as ‘most comfortable condition imaginable’
182 (Mündermann et al., 2003). Upon conclusion of the data collection, participants were also
183 asked to subjectively indicate which orthotic condition that they preferred.

184

185 To define the anatomical frames of the thorax, pelvis, thighs, shanks and feet retroreflective
186 markers were placed at the C7, T12 and xiphoid process landmarks and also positioned
187 bilaterally onto the acromion process, iliac crest, anterior superior iliac spine (ASIS),
188 posterior super iliac spine (PSIS), medial and lateral malleoli, medial and lateral femoral

189 epicondyles, greater trochanter, calcaneus, first metatarsal and fifth metatarsal. Carbon-fibre
190 tracking clusters comprising of four non-linear retroreflective markers were positioned onto
191 the thigh and shank segments. In addition to these, the foot segments were tracked via the
192 calcaneus, first metatarsal and fifth metatarsal, the pelvic segment was tracked using the PSIS
193 and ASIS markers and the thorax segment was tracked using the T12, C7 and xiphoid
194 markers. Static calibration trials were obtained with the participant in the anatomical position
195 in order for the positions of the anatomical markers to be referenced in relation to the tracking
196 clusters/markers. A static trial was conducted with the participant in the anatomical position
197 in order for the anatomical positions to be referenced in relation to the tracking markers,
198 following which those not required for dynamic data were removed.

199

200 To measure axially directed accelerations at the tibia, an accelerometer (Biometrics ACL 300,
201 Gwent United Kingdom) sampling at 1000Hz was used. The device was mounted onto a
202 piece of lightweight carbon-fibre material using the protocol outlined by Sinclair et al.,
203 (2013). The accelerometer was attached securely to the distal antero-medial aspect of the
204 tibia in alignment with its longitudinal axis, 0.08 m above the medial malleolus. Strong non-
205 stretch adhesive tape was placed over the device and leg to avoid overestimating the
206 acceleration due to tissue artefact (Sinclair et al., 2013).

207

208 The Achilles tendon of each participant's examined (right) side was inspected using
209 ultrasound imaging (SonoScope A6, Sonomed, China). Each participant laid face downwards
210 on a physiotherapy table with their ankle joint in a neutral position. A 46 mm 5-11 MHz
211 linear ultrasound probe (model L745) was placed perpendicular to the Achilles tendon,
212 between the medial and lateral malleoli (Milgrom et al., 2014). The medial-lateral and

213 anterior-posterior dimensions were recorded, and the cross-sectional area was calculated
214 using the associated formula for an oval i.e. Anterior-posterior * medial-lateral * $\pi / 4$
215 (Milgrom et al., 2014). Three images were obtained from each participant and the mean of
216 these recordings was calculated.

217

218 *Processing*

219 Dynamic trials were digitized using Qualisys Track Manager in order to identify anatomical
220 and tracking markers, then exported as C3D files to Visual 3D (C-Motion, Germantown, MD,
221 USA). All data were normalized to 100% of the stance phase then processed trials were
222 averaged within subjects for statistical analysis. Ground reaction force and kinematic data
223 were smoothed using cut-off frequencies of 50 and 12 Hz with a low-pass Butterworth 4th
224 order zero lag filter (Sinclair, 2018). All net force parameters throughout were normalized by
225 dividing by body mass (N/kg). Three-dimensional kinematic measures were extracted using
226 Visual 3D from the hip, knee, ankle that were extracted for statistical analysis were 1) angle
227 at footstrike, 2) peak angle during the stance phase and 3) angular range of motion (ROM)
228 from footstrike to peak angle. In addition, tibial internal rotation kinematics were also
229 calculated in accordance with Eslami et al., (2007). From the force platform, the external
230 instantaneous loading rate (N/kg/s) was calculated by obtaining the peak increase in force
231 between adjacent data points. In addition, the tibial acceleration signal was filtered using a 60
232 Hz Butterworth zero lag 4th order low pass filter (Sinclair et al., 2013), and the peak tibial
233 acceleration (g) was extracted as the highest positive acceleration peak during the stance
234 phase.

235

236 Data during the stance phase were exported from Visual 3D into OpenSim 3.3 software
237 (Simtk.org). A validated musculoskeletal model with 12 segments, 19 degrees of freedom
238 and 92 musculotendon actuators (Lerner et al., 2015) was used to estimate extremity joint
239 forces. The model was scaled for each participant to account for the anthropometrics of each
240 athlete. As muscle forces are the main determinant of joint compressive forces (Herzog et al.,
241 2003), muscle kinetics were quantified using static optimization. Peak compressive
242 patellofemoral, medial/ lateral tibiofemoral, ankle and hip joint forces were calculated via the
243 joint reaction analyses function using the muscle forces generated from the static
244 optimization process. Furthermore, peak patellofemoral stress (KPa/kg) was quantified by
245 dividing the patellofemoral force by the contact area. Patellofemoral contact areas were
246 obtained by fitting a polynomial curve to the sex specific data of Besier et al., (2005), who
247 estimated patellofemoral contact areas as a function of the knee flexion angle using MRI.

248

249 Achilles tendon forces were estimated in accordance with the protocol of Almonroeder et al.,
250 (2013), by summing the muscle forces of the medial gastrocnemius, lateral, gastrocnemius,
251 and soleus muscles. In addition, Achilles tendon stress was estimated by dividing the Achilles
252 tendon forces by the cross-sectional area of the tendon measured from the ultrasound images.
253 Peak Achilles tendon force (N/kg) and stress (KPa/kg) were extracted for statistical analysis.

254

255 In addition, patellofemoral, medial/ lateral tibiofemoral, ankle, hip and Achilles tendon
256 instantaneous load rates (N/kg/s and KPa/kg/s) were also extracted by obtaining the peak
257 increase in force/ stress between adjacent data points. Finally, the integral of the hip,
258 tibiofemoral, ankle, patellofemoral and Achilles tendon forces (N/kg·s) and stresses
259 (KPa/kg·s) during the stance phase were calculated using a trapezoidal function.

260

261 *Statistical analyses*

262 Descriptive statistics of means and standard deviations were obtained for each outcome
263 measure and for each orthotic condition. Shapiro-Wilk tests were used to screen the data for
264 normality. Differences in biomechanical parameters were examined using 5 (ORTHOTIC) x
265 2 (GENDER) mixed ANOVA's and differences in comfort ratings were examined using 4
266 (ORTHOTIC) x 2 (GENDER) mixed ANOVA's. Statistical significance was accepted at the
267 $P \leq 0.05$ level and effect sizes for all significant findings were calculated using partial Eta²
268 (η^2). In the event of a significant main effect, pairwise comparisons were performed.
269 Finally, a chi-squared (χ^2) test was utilised to test the assumption that an equal number of
270 participants would subjectively favour each of the orthotic conditions. All statistical actions
271 were conducted using SPSS v25.0 (SPSS Inc, Chicago, USA).

272

273 **Results**

274 *Joint kinetics*

275 **Medial tibiofemoral joint**

276 At the medial aspect of the **tibiofemoral** joint, there was a main effect of GENDER ($P < 0.05$,
277 $\eta^2 = 0.34$) for the peak medial tibiofemoral force, with peak force being greater in male
278 runners. In addition, there was a main effect of GENDER ($P < 0.05$, $\eta^2 = 0.33$) for the medial
279 tibiofemoral integral, with the medial tibiofemoral integral being greater in males.

280

281 **Lateral tibiofemoral joint**

282 At the lateral aspect of the tibiofemoral joint, there was a main effect of GENDER ($P < 0.05$,
283 $\eta^2 = 0.38$) for the peak lateral tibiofemoral force, with peak force being greater in male
284 runners. In addition, there was a main effect of ORTHOTIC ($P < 0.05$, $\eta^2 = 0.38$). Post-hoc
285 pairwise comparisons showed that the peak lateral tibiofemoral force was significantly
286 greater in the lateral ($P = 0.023$) condition, compared to the medial orthoses. In addition, there
287 was a main effect of GENDER ($P < 0.05$, $\eta^2 = 0.16$) for the lateral tibiofemoral instantaneous
288 loading rate, with this parameter being greater in male runners. In addition, there was a main
289 effect of ORTHOTIC ($P < 0.05$, $\eta^2 = 0.10$). Post-hoc pairwise comparisons showed that the
290 lateral tibiofemoral instantaneous loading rate was significantly greater in the lateral
291 ($P = 0.025$) condition, compared to the medial orthoses. Finally, there was a main effect of
292 GENDER ($P < 0.05$, $\eta^2 = 0.35$) for the lateral tibiofemoral force integral, with this value being
293 greater in male runners.

294

295 @@@TABLE 1 NEAR HERE@@@

296

297 Patellofemoral joint

298 A main effect of ORTHOTIC ($P < 0.05$, $\eta^2 = 0.09$) was found for peak patellofemoral force.
299 Post-hoc pairwise comparisons showed that peak patellofemoral force was significantly
300 larger in the lateral condition ($P = 0.039$) compared to the off the shelf orthoses. For peak
301 patellofemoral stress there was a main effect of ORTHOTIC ($P < 0.05$, $\eta^2 = 0.09$). Post-hoc
302 pairwise comparisons showed that peak patellofemoral stress was significantly larger in the
303 lateral condition ($P = 0.04$) compared to the off the shelf orthoses. In addition, there was also a
304 main effect of GENDER ($P < 0.05$, $\eta^2 = 0.35$), with peak stress being greater in females. For

305 the patellofemoral stress instantaneous loading rate, a main effect of GENDER ($P < 0.05$,
306 $p\eta^2 = 0.25$) was found, with this parameter being greater in females. For the patellofemoral
307 force integral a main effect of ORTHOTIC ($P < 0.05$, $p\eta^2 = 0.10$) was found. Post-hoc pairwise
308 comparisons showed that patellofemoral force integral was significantly larger in the lateral
309 condition, compared to no orthotic ($P = 0.04$) off the shelf orthoses ($P = 0.018$). There was also
310 a main effect of ORTHOTIC ($P < 0.05$, $p\eta^2 = 0.09$) for the patellofemoral stress integral. Post-
311 hoc pairwise comparisons showed that the patellofemoral stress integral was significantly
312 larger in the lateral condition ($P = 0.015$), compared to the off the shelf orthoses. In addition,
313 there was also a main effect of GENDER ($P < 0.05$, $p\eta^2 = 0.37$), the patellofemoral stress
314 integral being greater in females.

315

316 **Ankle joint**

317 At the ankle, there was a main effect of GENDER ($P < 0.05$, $p\eta^2 = 0.36$) for the peak ankle
318 force, with this measurement being larger in males. For the integral of the ankle force
319 ($P < 0.05$, $p\eta^2 = 0.24$), a main effect of GENDER was found, with the ankle force integral being
320 larger in males.

321

322 @@@TABLE 2 NEAR HERE@@@

323

324 **Achilles tendon kinetics**

325 There was a main effect of GENDER for both the peak Achilles tendon force ($P < 0.05$,
326 $p\eta^2 = 0.41$) and stress ($P < 0.05$, $p\eta^2 = 0.40$), with both parameters being greater in male runners.

327 In addition, there was a main effect of GENDER for both the Achilles tendon force ($P < 0.05$,
328 $\eta^2 = 0.36$) and stress ($P < 0.05$, $\eta^2 = 0.35$) instantaneous loading rates, with both parameters
329 being greater in male runners. Finally, for the integral of the Achilles tendon force ($P < 0.05$,
330 $\eta^2 = 0.18$) and stress ($P < 0.05$, $\eta^2 = 0.19$), a main effect of GENDER was found, with both
331 measures being larger in males.

332

333 *External instantaneous loading rate and tibial accelerations*

334 For the external instantaneous loading rate, there was a main effect for ORTHOTIC ($P < 0.05$,
335 $\eta^2 = 0.10$). Post-hoc pairwise comparisons showed that the instantaneous loading rate was
336 significantly greater in the medial ($P = 0.028$) and semi-custom ($P = 0.03$) conditions compared
337 to the off the shelf orthoses. For peak tibial acceleration, there was a main effect for
338 ORTHOTIC ($P < 0.05$, $\eta^2 = 0.11$). Post-hoc pairwise comparisons showed that the peak tibial
339 accelerations were significantly greater in the semi-custom ($P < 0.001$) conditions compared to
340 the off the shelf orthoses. In addition, there was also a main effect of GENDER ($P < 0.05$, η^2
341 $= 0.13$), with tibial accelerations being greater in females.

342

343 *Subjective ratings*

344 There was a main effect of ORTHOTIC ($P < 0.05$, $\eta^2 = 0.51$) for participants ratings of
345 comfort. Post-hoc pairwise comparisons showed that the semi-custom ($P < 0.001$ & $P < 0.001$)
346 and off the shelf ($P < 0.001$ & $P < 0.001$) orthoses were rated as being significantly more
347 comfortable than the medial and lateral conditions. Finally, the semi-custom orthoses were
348 rated as being significantly ($P = 0.029$) more comfortable than the off the shelf condition. In
349 addition, the Chi-squared analysis of orthotic preferences was significant ($\chi^2_{(3)} = 22.00$,

350 P<0.05) with 19 participants selecting the semi-custom orthoses, 12 off the shelf, 4 medial
351 and 1 the lateral conditions.

352

353 **@@@TABLE 3 NEAR HERE@@@**

354

355 *Joint kinematics*

356 **Hip**

357 For the peak hip adduction angle there was a main effect of ORTHOTIC ($P<0.05$, $\eta^2=0.20$).
358 Post-hoc pairwise comparisons showed that peak adduction was significantly greater in the
359 lateral and semi-custom orthoses compared to the medial ($P<0.001$ & $P=0.002$), no orthotic
360 ($P=0.002$ & $P=0.036$) and off the shelf orthoses ($P<0.001$ & $P<0.001$). There was also a main
361 effect of GENDER ($P<0.05$, $\eta^2=0.14$), with peak adduction being larger in females.

362

363 **Knee**

364 For the sagittal knee angle at footstrike there was a main effect of GENDER ($P<0.05$,
365 $\eta^2=0.18$), with knee flexion being larger in females. There was also a main effect of
366 GENDER ($P<0.05$, $\eta^2=0.20$) for the peak knee flexion angle, which was shown to be greater
367 in females. There was also a main effect of ORTHOTIC ($P<0.05$, $\eta^2=0.11$) for the peak
368 knee abduction angle. Post-hoc pairwise comparisons showed that peak abduction was
369 significantly larger in the lateral ($P=0.032$) and semi-custom orthoses ($P=0.01$) compared to
370 the no orthotic condition.

371

372 **Ankle**

373 For the sagittal ankle angle at footstrike there was a main effect of GENDER ($P < 0.05$,
374 $\eta^2 = 0.25$), with dorsiflexion being larger in females. In addition, there was also a main effect
375 of ORTHOTIC ($P < 0.05$, $\eta^2 = 0.13$) for the peak dorsiflexion angle. Post-hoc pairwise
376 comparisons showed that peak dorsiflexion was significantly greater in the medial orthoses
377 compared to the lateral ($P = 0.04$), no orthotic ($P = 0.028$), off the shelf ($P = 0.012$) and semi-
378 custom ($P = 0.01$) conditions. There was also a main effect of GENDER ($P < 0.05$, $\eta^2 = 0.22$)
379 for dorsiflexion ROM, with this measurement being larger in males.

380

381 For the peak eversion angle there was a main effect of ORTHOTIC ($P < 0.05$, $\eta^2 = 0.26$). Post-
382 hoc pairwise comparisons showed that peak eversion was significantly greater in the lateral
383 ($P < 0.001$), no orthotic ($P < 0.001$), off the shelf ($P < 0.032$) and semi-custom ($P < 0.001$)
384 conditions compared to medial orthoses. In addition, for the eversion ROM there was a main
385 effect of ORTHOTIC ($P < 0.05$, $\eta^2 = 0.61$). Post-hoc pairwise comparisons showed that
386 eversion ROM was significantly greater in the lateral ($P < 0.001$), no orthotic ($P < 0.001$), off
387 the shelf ($P < 0.001$) and semi-custom ($P < 0.001$) conditions compared to the medial orthoses.
388 In addition, peak eversion was significantly larger in the lateral orthoses compared to the off
389 the shelf ($P < 0.001$), semi-custom ($P < 0.001$) and no orthotic ($P = 0.005$) conditions.

390

391 **Tibial internal rotation**

392 For the peak tibial internal rotation angle there was a main effect of ORTHOTIC ($P < 0.05$,
393 $\eta^2 = 0.28$). Post-hoc pairwise comparisons showed that peak tibial internal rotation was
394 significantly greater in the lateral orthoses compared to the medial ($P < 0.001$) no orthotic

395 (P<0.001), off the shelf (P<0.001) and semi-custom (P<0.017) conditions. In addition, peak
396 tibial internal rotation was significantly greater in the semi-custom orthoses compared to the
397 medial (P<0.001) and off the shelf (P=0.001) conditions. In addition, for the tibial internal
398 rotation ROM there was a main effect of ORTHOTIC (P<0.05, $\eta^2=0.30$). Post-hoc pairwise
399 comparisons showed that tibial internal rotation ROM was significantly greater in the lateral
400 (P<0.001), no orthotic (P<0.001), off the shelf (P=0.001) and semi-custom (P<0.001)
401 conditions compared to the medial orthoses. In addition, tibial internal rotation ROM was
402 also significantly greater in the lateral (P=0.04), no orthotic (P=0.027) and semi-custom
403 orthoses (P=0.001) compared to the off the shelf condition.

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409 **Discussion**

410 This study aimed to examine the effects of different orthotic conditions on the biomechanical
411 mechanisms linked to the aetiology of chronic pathologies. To the authors knowledge this is
412 the first investigation to collectively explore the effects of different orthoses on lower
413 extremity kinetics and kinematics during running, and may provide insight into the potential
414 efficacy of different foot orthoses for the prevention chronic running pathologies.

415

416 Patellofemoral pain is regarded as the most common chronic running injury (Taunton et al.,
417 2002). Females are renowned for being at increased risk from patellofemoral disorders;
418 therefore, it is important that the current investigation showed female runners to be associated
419 with increased patellofemoral loading. This observation concurs with those of Sinclair &
420 Selfe, (2015) and given the proposed relationship between joint stress and patellofemoral
421 pathology (Farrokhi et al., 2011), appears to provide insight into the responsible factors for
422 the increased incidence of patellofemoral pain in females. In support of the findings of
423 Sinclair, (2018), the current investigation also showed that patellofemoral joint stress
424 parameters were significantly greater when running in the lateral orthoses in relation to
425 running in off the shelf devices. Although the mean difference between these orthotic
426 conditions was relatively small, this observation may nonetheless be clinically important, as
427 patellofemoral pain symptoms are believed to be initiated via excessive/ repeated
428 patellofemoral joint stress (Farrokhi et al., 2011). The current study indicates that running
429 with off the shelf orthoses may be preferable over lateral wedged devices, as a mechanism to
430 reduce the risk from the biomechanical parameters linked to the aetiology of patellofemoral
431 pain in runners.

432

433 At the tibiofemoral joint, there was no effect of orthoses at the medial aspect. This opposes
434 previous walking analyses, which have consistently shown that lateral orthoses reduce the
435 magnitude of the external knee adduction moment (Jones et al., 2013). It is proposed that the
436 difference between analyses relates to the manner in which tibiofemoral loading was
437 calculated in the current study, as previous analyses have used coronal plane joint torques as
438 a pseudo measure of medial compartment loading, which do not account for muscular co-
439 contraction about the knee joint (Herzog et al., 2003). However, at the lateral aspect of the
440 tibiofemoral joint compressive loading was significantly greater in the lateral orthoses in

441 relation to the medial devices. This indicates that although lateral orthoses were not able to
442 attenuate compressive loading at the medial aspect of the joint, they were able to transfer load
443 to the lateral tibiofemoral compartment. Therefore, although the increases in compressive
444 load were small, lateral wedged devices may place runners at greater risk from the
445 mechanisms associated with tibiofemoral pathologies. Furthermore, in contrast, to the
446 findings at the patellofemoral joint, this investigation showed that at both the medial and
447 lateral aspects of the tibiofemoral joint males were associated with statistically greater joint
448 loading parameters in relation to females. Leading to the conclusion that males are at greater
449 risk from the biomechanical parameters linked to the aetiology of tibiofemoral pathologies.

450

451 In agreement with the findings of Greenhalgh & Sinclair, (2014) the current study also
452 showed that males were associated with increased Achilles tendon stress and ankle joint force
453 parameters. In contrast to patellofemoral pathologies, males are at increased risk from
454 Achilles tendinopathies in relation to age-matched females (Hess, 2010). Given the proposed
455 association between tendon stress and the physiological initiation of tendinous collagen
456 degradation (Abate et al., 2009), this observation appears to provide further insight into the
457 biomechanical mechanisms behind the increased incidence Achilles tendinopathy in males.
458 However, as there were no significant differences between orthoses in ankle or Achilles
459 tendon load parameters, the observations from this investigation are in contrast to those of
460 Sinclair et al., (2014) who showed that off the shelf orthoses significantly reduced peak
461 Achilles tendon force, but agree with those of Sinclair et al., (2015) with regards to semi-
462 custom devices. As such, the findings from this study using musculoskeletal simulation
463 indicate that foot orthoses do not influence the biomechanical parameters linked to the
464 aetiology of ankle/ Achilles tendon pathologies during running.

465

466 Importantly, in agreement with the findings of Mündermann et al., (2003) and Sinclair et al.,
467 (2014), this study also showed that instantaneous loading rates and peak tibial accelerations
468 were significantly larger in the medial and semi-custom conditions compared to off the shelf
469 orthoses. Excessive tibial accelerations/ vertical rates of loading are the biomechanical
470 mechanisms responsible for the development of stress fractures (Warden et al., 2006).

471 Therefore, this study indicates that off the shelf orthoses may be effective in attenuating the
472 mechanisms linked to the aetiology of tibial stress fractures in runners. In addition, that
473 females were associated with increased tibial accelerations may also be clinically important
474 taking into account their proposed link to the aetiology of stress fractures and may provide
475 further insight into the biomechanical mechanisms responsible for the increased incidence of
476 stress fractures in female runners (Jones et al., 1993).

477

478 In conclusion, although the biomechanical effects of foot orthoses have been examined
479 previously, current knowledge with regards to the effects of different orthoses is limited. This
480 study therefore adds to the current literature by examining the influence of different orthoses
481 on the biomechanical mechanisms linked to the aetiology of chronic pathologies, using
482 musculoskeletal simulation. The current investigation importantly showed that patellofemoral
483 stress parameters and loading rates/ peak tibial accelerations were significantly reduced in the
484 off the shelf orthoses and lateral tibiofemoral loading parameters were significantly
485 attenuated in the medial orthotic condition. Therefore, the current investigation indicates that
486 different orthotic devices/ configurations may provide distinct benefits in terms of their
487 effectiveness in attenuating the biomechanical parameters linked to the aetiology of chronic
488 running injuries.

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611 Table 1: Hip and knee joint kinetics (Mean & SD) for each orthotic condition.

	Male										
	Medial		Lateral		No-orthoses		Semi-custom		Off the shelf		
	Mean	SD	Mean	SD	Mean	SD	Mean	SD	Mean	SD	
Peak hip force (N/kg)	88.48	7.32	90.33	8.34	89.99	8.29	91.42	10.18	87.97	8.18	
Hip force instantaneous load rate (N/kg/s)	3307.86	913.51	3315.23	669.65	3828.30	786.74	3839.14	1117.64	3589.09	803.50	
Hip integral (N/kg·s)	13.03	1.79	13.55	1.77	13.25	1.88	13.17	2.02	12.95	1.58	
Peak medial tibiofemoral force (N/kg)	71.02	8.45	73.66	9.70	71.79	9.71	71.24	12.16	74.79	9.95	B
Medial tibiofemoral instantaneous load rate (N/kg/s)	2434.42	536.84	2591.40	567.63	2914.90	850.45	2599.01	894.05	2475.01	771.44	
Medial tibiofemoral integral (N/kg·s)	9.03	1.15	9.37	1.23	9.13	1.30	9.09	1.51	9.16	1.07	B
Peak lateral tibiofemoral force (N/kg)	45.44	12.53	48.04	14.86	48.93	14.44	49.37	16.16	48.50	11.15	A, B
Lateral tibiofemoral instantaneous load rate (N/kg/s)	1773.79	583.72	1959.83	679.00	1849.62	598.64	1947.66	690.18	1859.87	466.90	A, B
Lateral tibiofemoral integral (N/kg·s)	4.68	0.85	4.59	1.20	4.67	0.91	4.72	1.12	4.78	0.77	B
	Female										
	Medial		Lateral		No-orthoses		Semi-custom		Off the shelf		
	Mean	SD	Mean	SD	Mean	SD	Mean	SD	Mean	SD	
Peak hip force (N/kg)	84.75	8.47	85.26	8.48	85.36	10.78	86.45	9.85	85.43	8.15	
Hip force instantaneous load rate (N/kg/s)	3285.00	882.75	3281.45	799.94	3010.18	588.48	3396.73	1042.38	3387.98	1122.21	
Hip integral (N/kg·s)	11.82	1.60	12.43	1.22	12.03	1.63	12.33	1.58	11.93	1.50	
Peak medial tibiofemoral force (N/kg)	60.20	13.01	58.56	9.76	57.27	13.15	59.59	10.91	58.97	10.95	B
Medial tibiofemoral instantaneous load rate	2529.12	1153.93	2542.29	995.54	2346.42	802.95	2482.47	932.52	2425.37	975.89	

(N/kg/s)											
Medial tibiofemoral integral (N/kg·s)	7.29	1.44	7.49	1.42	7.25	1.75	7.44	1.62	7.25	1.62	B
Peak lateral tibiofemoral force (N/kg)	32.66	7.41	35.54	6.59	34.52	8.38	34.98	7.89	32.50	6.65	A, B
Lateral tibiofemoral instantaneous load rate (N/kg/s)	1428.72	406.22	1616.61	483.48	1523.92	521.47	1578.85	461.88	1374.27	306.65	A, B
Lateral tibiofemoral integral (N/kg·s)	3.51	0.83	3.76	0.86	3.56	0.95	3.62	0.84	3.42	0.72	B

Key: A = main effect of ORTHOSES & B = main effect of GENDER

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629 Table 2: Patellofemoral and joint kinetics (Mean & SD) for each orthotic condition.

	Male										
	Medial		Lateral		No-orthoses		Semi-custom		Off the shelf		
	Mean	SD	Mean	SD	Mean	SD	Mean	SD	Mean	SD	
Peak ankle force (N/kg)	115.69	22.41	118.63	15.40	117.87	19.59	121.14	21.30	120.16	15.85	B
Ankle force instantaneous load rate (N/kg/s)	3129.58	1059.63	3218.30	649.58	3334.58	941.19	3227.41	509.45	3148.57	656.10	
Ankle integral (N/kg-s)	13.48	2.61	13.95	1.65	13.75	2.35	14.39	2.67	14.08	2.13	B
Peak patellofemoral force (N/kg)	40.26	14.78	40.54	16.90	39.00	13.16	40.01	14.42	39.14	13.50	A
Peak patellofemoral stress (KPa/kg)	70.56	22.11	70.49	25.69	68.92	19.93	70.15	21.80	68.55	20.63	A, B
Patellofemoral force instantaneous load rate (N/kg/s)	1272.87	339.23	1274.20	339.02	1306.85	380.22	1310.70	336.69	1217.09	268.24	
Patellofemoral stress instantaneous load rate (KPa/kg/s)	2466.63	585.35	2477.26	429.23	2782.31	877.60	2721.66	588.61	2506.96	602.10	B
Patellofemoral force integral (N/kg-s)	3.10	1.31	3.33	1.73	2.95	1.13	3.03	1.35	3.13	1.28	A
Patellofemoral stress integral (KPa/kg-s)	5.60	2.11	5.90	2.83	5.40	1.89	5.50	2.22	5.60	2.08	A, B
	Female										
	Medial		Lateral		No-orthoses		Semi-custom		Off the shelf		
	Mean	SD	Mean	SD	Mean	SD	Mean	SD	Mean	SD	
Peak ankle force (N/kg)	96.42	16.52	98.71	12.73	98.83	16.37	97.52	17.63	95.96	14.61	B
Ankle force instantaneous load rate (N/kg/s)	3013.14	736.42	3020.20	631.00	2817.86	679.30	3028.02	681.18	2960.76	789.04	
Ankle integral (N/kg-s)	11.72	2.05	12.05	1.84	11.73	2.25	11.83	2.30	11.62	1.87	B
Peak patellofemoral force (N/kg)	46.86	14.56	48.56	12.39	44.59	10.83	49.01	16.86	44.39	11.53	A
Peak patellofemoral stress (KPa/kg)	100.28	24.13	103.22	20.69	96.57	17.88	104.41	30.19	94.91	18.83	A, B

Patellofemoral force instantaneous load rate (N/kg/s)	1473.54	521.20	1423.69	409.31	1388.64	517.25	1390.18	354.61	1367.60	486.44	
Patellofemoral stress instantaneous load rate (KPa/kg/s)	3785.04	1398.42	3633.07	1118.76	3658.16	1305.26	3667.80	949.96	3584.23	1450.64	B
Patellofemoral force integral (N/kg·s)	4.01	1.43	4.15	1.20	3.89	1.33	4.14	1.74	3.76	1.31	A
Patellofemoral stress integral (KPa/kg·s)	9.00	2.55	9.30	2.03	8.80	2.28	9.30	3.25	8.50	2.32	A, B

Key: A = main effect of ORTHOSES & B = main effect of GENDER

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648 Table 3: Achilles tendon, loading rate and tibial acceleration parameters (Mean & SD) for each
649 orthotic condition.

	Medial		Lateral		No-orthoses		Semi-custom		Off the shelf		
	Mean	SD	Mean	SD	Mean	SD	Mean	SD	Mean	SD	
Comfort	5.92	2.91	6.00	3.33			11.83	2.21	10.33	3.20	A
External instantaneous load rate (N/kg/s)	1480.45	525.84	1383.08	356.07	1562.52	431.02	1552.99	419.77	1290.60	395.12	A
Peak tibial acceleration (g)	7.09	2.26	7.35	1.95	7.07	1.88	7.93	1.94	6.91	1.71	A, B
Peak Achilles tendon force (N/kg)	75.54	10.23	75.77	6.75	76.19	14.36	77.77	13.95	78.64	11.56	B
Peak Achilles tendon stress (KPa/kg)	1569.68	212.50	1574.58	140.27	1583.26	298.50	1616.16	289.90	1634.15	240.26	B
Achilles tendon instantaneous load rate (N/kg/s)	1650.18	445.92	1539.91	239.20	1703.98	550.80	1587.40	309.96	1632.10	415.57	B
Achilles tendon stress instantaneous load rate (KPa/kg/s)	34290.99	9266.24	31999.52	4970.71	35408.90	11445.66	32986.31	6440.98	33915.23	8635.62	B
Achilles tendon force integral (N/kg·s)	7.80	1.42	7.94	0.74	7.84	1.88	8.26	1.72	8.19	1.46	B
Achilles tendon stress integral (KPa/kg·s)	162.13	29.53	164.96	15.45	162.93	39.17	171.60	35.68	170.27	30.30	B
	Female										
	Medial		Lateral		No-orthoses		Semi-custom		Off the shelf		
	Mean	SD	Mean	SD	Mean	SD	Mean	SD	Mean	SD	
Comfort	5.45	3.91	6.65	3.45			11.95	3.32	10.45	2.87	A
External instantaneous load rate (N/kg/s)	1767.05	950.24	1629.06	600.96	1669.17	648.25	1704.37	526.02	1567.10	712.42	A
Peak tibial acceleration (g)	8.72	2.15	8.90	2.21	8.70	2.42	9.01	2.12	8.55	2.09	A, B
Peak Achilles tendon force (N/kg)	61.53	12.32	61.39	10.86	60.93	11.67	61.96	12.60	60.89	10.26	B
Peak Achilles tendon stress (KPa/kg)	1278.52	255.94	1275.66	225.70	1266.16	242.42	1287.52	261.73	1265.29	213.26	B
Achilles tendon instantaneous load rate (N/kg/s)	1285.07	327.89	1211.65	244.72	1136.86	270.52	1286.43	348.36	1244.78	322.38	B
Achilles tendon stress instantaneous load rate	26703.86	6813.52	25178.27	5085.26	23624.08	5621.48	26732.19	7239.00	25866.78	6699.04	B

(KPa/kg/s)											
Achilles tendon force integral (N/kg·s)	6.81	1.61	6.84	1.40	6.66	1.66	6.82	1.66	6.70	1.34	B
Achilles tendon stress integral (KPa/kg·s)	141.50	33.37	142.06	29.11	138.40	34.40	141.64	34.43	139.33	27.75	B

Key: A = main effect of ORTHOSES & B = main effect of GENDER

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669 Table 4: Three-dimensional hip joint kinematics (Mean & SD) for each orthotic condition.

	Male										
	Medial		Lateral		No-orthoses		Semi-custom		Off the shelf		
	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	
Sagittal plane											
Angle at footstrike (°)	38.15	14.28	39.36	13.40	38.07	14.42	40.77	8.41	37.69	12.84	
Peak flexion (°)	38.77	14.08	39.90	13.32	38.34	14.04	41.20	8.26	38.33	12.33	
ROM (°)	0.62	1.26	0.54	1.04	0.28	0.60	0.43	0.67	0.63	1.06	
Coronal plane											
Angle at footstrike (°)	-0.04	8.99	1.02	8.93	0.07	9.69	1.64	6.75	-0.21	9.05	
Peak adduction (°)	7.77	8.57	9.18	7.79	7.70	8.68	9.75	5.98	7.41	7.65	A, B
ROM (°)	7.81	5.40	8.16	4.59	7.63	4.02	8.11	4.21	7.62	3.89	
Transverse plane											
Angle at footstrike (°)	4.54	11.41	3.33	11.42	6.03	10.87	3.19	12.37	3.97	11.71	
Peak external rotation (°)	-7.67	12.12	-7.43	12.63	-5.91	11.27	-9.01	12.78	-7.57	12.76	
ROM (°)	12.22	6.11	10.76	6.29	11.95	6.70	12.20	6.55	11.54	5.06	
	Female										
	Medial		Lateral		No-orthoses		Semi-custom		Off the shelf		
	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	
Sagittal plane											
Angle at footstrike (°)	46.66	9.69	47.82	11.08	46.53	10.75	46.03	12.02	46.24	11.90	
Peak flexion (°)	47.15	9.52	48.41	10.56	47.05	10.00	47.00	11.04	47.07	10.84	
ROM (°)	0.49	0.86	0.59	1.20	0.52	1.35	0.97	1.92	0.83	2.19	
Coronal plane											
Angle at footstrike (°)	4.75	5.87	4.40	5.76	3.56	6.23	3.70	5.99	3.78	5.62	
Peak adduction (°)	12.42	4.93	14.18	4.39	12.73	4.65	13.31	4.35	12.25	4.24	A, B
ROM (°)	7.67	3.05	9.78	4.00	9.17	3.53	9.61	3.74	8.47	4.01	
Transverse plane											
Angle at footstrike (°)	10.86	8.21	10.52	8.32	10.01	7.35	10.06	8.92	11.23	8.97	

Peak external rotation (°)	-2.66	7.98	-3.12	7.96	-1.68	7.72	-3.33	7.73	-2.80	8.11	
ROM (°)	13.52	6.42	13.63	6.67	11.69	6.30	13.39	6.54	14.04	7.54	

670 Key: A = main effect of ORTHOSES & B = main effect of GENDER

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693 Table 5: Three-dimensional knee joint kinematics (Mean & SD) for each orthotic condition

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	Medial		Lateral		No-orthoses		Semi-custom		Off the shelf		
	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	
Sagittal plane											
Angle at footstrike (°)	14.66	5.66	16.21	6.05	13.92	6.54	15.27	6.29	14.34	6.64	B
Peak flexion (°)	43.35	6.04	44.28	6.05	42.71	5.89	43.79	5.13	43.48	5.76	B
ROM (°)	28.69	4.70	28.07	4.33	28.79	4.94	28.52	6.05	29.14	4.83	
Coronal plane											
Angle at footstrike (°)	1.22	4.96	1.06	4.15	1.58	4.96	0.44	4.55	1.60	4.82	
Peak adduction (°)	-5.96	5.37	-6.24	5.67	-5.27	4.85	-6.64	5.48	-5.49	5.33	A
ROM (°)	7.18	3.06	7.29	3.69	6.85	4.05	7.07	3.02	7.09	2.60	
Transverse plane											
Angle at footstrike (°)	-12.87	8.16	-11.55	6.23	-15.75	7.95	-11.96	8.11	-13.42	8.55	
Peak external rotation (°)	7.50	9.35	8.24	9.18	8.01	8.54	8.36	9.80	7.96	8.78	
ROM (°)	20.38	5.41	19.80	6.16	23.76	5.73	20.32	6.95	21.38	5.75	
	Female										
	Medial		Lateral		No-orthoses		Semi-custom		Off the shelf		
	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	<i>Mean</i>	<i>SD</i>	
Sagittal plane											
Angle at footstrike (°)	22.57	7.86	22.47	8.14	22.85	9.89	20.63	9.46	21.37	9.58	B
Peak flexion (°)	49.92	7.93	50.79	6.93	49.19	7.06	50.26	7.66	49.75	7.52	B
ROM (°)	27.35	6.68	28.32	6.90	26.34	7.86	29.62	7.77	28.38	8.40	
Coronal plane											
Angle at footstrike (°)	0.86	5.54	1.03	6.04	1.57	5.87	0.63	5.61	1.07	5.78	
Peak adduction (°)	-6.89	4.76	-7.31	5.18	-6.19	3.65	-7.14	4.78	-6.86	4.49	A
ROM (°)	7.75	4.37	8.34	4.79	7.76	4.75	7.76	4.45	7.93	4.85	
Transverse plane											
Angle at footstrike (°)	-11.93	4.86	-12.41	7.30	-10.95	5.51	-11.46	6.97	-11.84	6.57	
Peak external rotation (°)	3.63	5.74	4.13	6.01	3.79	5.94	4.30	6.06	4.28	5.59	

ROM (°)	15.57	5.78	16.54	6.12	14.73	6.11	15.76	6.36	16.12	6.94	
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715 Key: A = main effect of ORTHOSES & B = main effect of GENDER

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738 Table 6: Three-dimensional ankle joint kinematics (Mean & SD) for each orthotic condition.

Angle at footstrike (°)	-0.95	5.67	3.56	6.44	2.61	5.03	2.89	5.85	1.78	5.63	
Peak eversion (°)	-7.72	4.75	-10.32	5.61	-10.10	4.04	-9.49	5.93	-8.85	4.98	A
ROM (°)	6.77	3.45	13.88	4.38	12.71	3.37	12.38	4.41	10.63	4.08	A
Transverse plane											
Angle at footstrike (°)	-4.08	6.77	-4.89	7.03	-3.30	6.89	-3.48	6.21	-3.75	6.22	
Peak external rotation (°)	-8.27	7.73	-10.44	7.21	-9.22	7.30	-10.10	7.37	-9.06	6.64	
ROM (°)	4.19	3.09	5.55	2.93	5.92	3.64	6.62	3.56	5.31	3.25	
Tibial internal rotation at footstrike (°)	11.84	6.19	11.96	6.47	10.66	6.73	10.62	6.53	10.97	5.72	
Peak tibial internal rotation (°)	16.99	6.56	19.84	6.00	18.28	6.07	19.13	6.08	18.01	5.36	A
Peak tibial internal rotation ROM (°)	5.15	3.07	7.88	2.85	7.62	3.31	8.51	3.21	7.04	3.14	A

Key: A = main effect of ORTHOSES & B = main effect of GENDER