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1	Effects of running with minimal and conventional footwear in habitual and non-
2	habitual users; a musculoskeletal simulation and statistical parametric mapping based
3	<mark>approach.</mark>
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9	Keywords: Biomechanics; musculoskeletal; footwear; running, minimal footwear.
10 11	Abstract
12	The current investigation examined running biomechanics in minimal and conventional
13	footwear in two groups of runners who either ran habitually in minimal footwear (habitual
14	minimal footwear users) or habitually in conventional footwear (non-habitual minimal footwear
15	users). We studied ten male non-habitual minimal footwear users and ten male habitual minimal
16	footwear users, who were required to complete \geq 35 km per week of training. Lower extremity
17	joint loading was explored using a musculoskeletal simulation approach. Differences between
18	conditions were examined using statistical parametric mapping and 2x2 mixed ANOVA. This
19	study revealed via the strike index that minimal footwear caused a more anterior contact
20	position in both groups (habitual: minimal=61.68% & conventional=46.48% /non-habitual:
21	minimal=33.79% & conventional=22.61%), although non-habitual runners still adopted a
22	rearfoot strike pattern. In addition, in non-habitual users minimal footwear increased tibial
23	accelerations (habitual: minimal=6.35g & conventional=7.06g /non-habitual: minimal=9.54g
24	& conventional=8.16g), loading rates (habitual: minimal=105.44BW/s &

conventional=105.97BW/s /non-habitual: minimal=293.00BW/s 25 & medial tibiofemoral conventional=154.36BW/s) and loading (habitual: 26 rates minimal=196.17BW/s & conventional=274.96BW/s /non-habitual: minimal=274.96BW/s & 27 conventional=212.57BW/s). Furthermore, minimal footwear decreased patellofemoral loading 28 both habitual (minimal=0.28BW·s & conventional=0.31BW·s) and non-habitual 29 in (minimal=0.26BW·s & conventional=0.29BW·s) users. Finally, Achilles tendon loading was 30 larger in minimal footwear and in habitual runners (habitual: minimal=0.79BW·s & 31 conventional=0.71BW·s /non-habitual: minimal=0.71BW·s & conventional=0.65BW·s) 32 33 whereas iliotibial band strain rate was reduced in habitual (minimal=28.32%/s & conventional=30.30%/s) relation non-habitual (minimal=42.96%/s)& 34 in to conventional=42.87%/s) users. This study highlights firstly the importance of transitioning to 35 minimal footwear and also indicates that post transition they may be effective in attenuating the 36 biomechanical mechanisms linked to the aetiology of many chronic injuries. 37

38

39 Introduction

Recreational distance running is arguably the most popular aerobic exercise modality (Lee et 40 al. 2014). There is a plethora of evidence indicating that running mediates significant 41 physiological and psychological benefits (Lee et al. 2014). However, despite the physical 42 benefits that it manifests, distance running is also associated with a high susceptibility to 43 44 chronic injuries; as 19.4-79.3 % of runners will experience a pathology each year (Van Gent et al. 2007). Unfortunately, chronic pathologies are a significant barrier to training adherence in 45 runners and lead to a substantial economic burden (Hespanhol et al. 2016). Specifically, 46 patellofemoral pain, iliotibial band syndrome, tibial stress fractures, medial tibial stress 47 syndrome, Achilles tendinopathy and pain secondary to hip and knee osteoarthritis are 48

commonly experienced in sports medicine clinics (Taunton et al. 2002, Van Ginckel et al. 2009;
Winkelmann et al. 2016; Snyder et al. 2006).

51

The running shoe is the primary interface between the body and surface; as such significant 52 developments in running shoe technology have emerged, in an attempt to mediate the incidence 53 of chronic running pathologies (Sinclair et al. 2013a). However, since the introduction of the 54 conventional running shoe, the rate and location of chronic running injuries has not changed, 55 leading to the notion that technological developments in running footwear have not been 56 successful in influencing running pathologies (Davis, 2014). This has led to the proposal that 57 58 running in minimal footwear that lacks the cushioning and motion control properties associated 59 with the conventional running shoe, may be associated with a reduced incidence of chronic running injuries (Lieberman et al. 2010; Davis, 2014). Based on this notion, several minimal 60 footwear models are currently available commercially. 61

62

63 Several studies have examined differences in running biomechanics between minimal and conventional running shoes. These investigations have shown that minimal footwear alter 64 spatiotemporal running characteristics, causing runners to adopt a more plantarflexed ankle at 65 footstrike (Sinclair et al. 2013ab, Hollander et al. 2015), mid/forefoot strike pattern (Squadrone 66 et al. 2015; Sinclair et al. 2019), increased stride rate (Warne et al. 2014) and reduced stride 67 length (Sinclair et al. 2016; Sinclair et al. 2019) compared to conventional running shoes. In 68 addition, previous comparisons of conventional and minimal footwear have also shown that 69 70 minimal footwear are associated with increased vertical loading rates (Sinclair et al. 2013ab), tibial accelerations (Sinclair et al. 2013a), and effective mass (Sinclair et al. 2018a). Finally, 71 previous work examining the effects of minimal footwear on the loads experienced by the lower 72 73 extremities have revealed that minimal footwear reduces the loads experienced by the

74	patellofemoral joint (Sinclair, 2014; Bonacci et al. 2014), but increase the forces borne by the
75	Achilles tendon (Sinclair, 2014; Sinclair et al. 2019) and the tibiofemoral joint (Sinclair et al.
76	2018b). However, it is important to recognise that the conclusions drawn from the
77	aforementioned investigations were based upon results obtained from novice users of minimal
78	footwear. Indeed, Tam et al. (2017) proposed that in acute investigations of minimal footwear,
79	runners do not sufficiently alter their running mechanics sufficiently to reduce the vertical
80	loading rate. Therefore, it can be concluded that the overall evidence that minimal footwear is
81	able to attenuate the biomechanical factors linked to the aetiology of chronic pathologies is
82	currently insufficient. As such, with regards to minimal footwear, runners must select footwear
83	based on the findings from acute studies conducted on runners who are unaccustomed to using
84	minimal footwear. Therefore, it can be concluded that further investigation of running
85	biomechanics between minimal and conventional footwear in those who habitually wear
86	minimal and conventional footwear is warranted.
87	
88	Furthermore, previous analyses concerning the biomechanical differences between minimal
89	and conventional footwear, have adopted inverse-dynamic driven modelling-based approaches
90	to quantify lower extremity musculoskeletal loading (Sinclair et al., 2019). However, joint
91	torques are representative of global indices of joint loading, and therefore are not representative
92	of localized joint loading (Herzog et al. 2003). Substantial developments in musculoskeletal
93	modelling have been made in recent years, allowing indices of skeletal muscle forces; muscle
94	kinematics and joint reaction forces be obtained through musculoskeletal simulation analyses
95	(Delp et al. 2007). This approach may be more effective than traditional inverse-dynamic based
96	methods and allows a more detailed examination of the specific parameters linked to the
97	aetiology of chronic pathologies to be undertaken. Such approaches have not yet been utilized

99	runners	who	run	habitually	in	minimal	footwear	(habitual	minimal	footwear	users)	01
100	convent	ional f	footw	vear (non-h	abit	ual minim	al footwea	r users).				

101

There has yet to be a published investigation examining differences in running biomechanics between minimal and conventional footwear in those who habitually wear minimal and conventional footwear. Therefore, the aim of the current investigation was to examine running biomechanics in minimal and conventional footwear in those who habitually wear minimal and conventional footwear, with reference to the biomechanical mechanisms linked to the aetiology of chronic pathologies, using a musculoskeletal simulation-based analysis.

108

114

- 109 Methods
- 110 Participants

111	Ten male	conventional	footwear	users	(henceforth	termed	non-habitual	minimal	footwear

users) (age 27.67 \pm 5.57 years, height 1.71 \pm 0.03 m and body mass 68.76 \pm 4.78 kg) and ten

113 male habitual minimal footwear users (henceforth termed habitual minimal footwear users)

115 take part in this study. Participants were required to complete a minimum of 35 km per week

(age 33.50 \pm 4.58 years, height 1.75 \pm 0.04 m and body mass 71.74 \pm 7.74 kg) volunteered to

116 of training. To be considered a habitual minimal footwear user, volunteers were required to

117 have been training exclusively in minimal footwear for a minimum period of 24 months in

118 footwear scoring \geq 75 on the minimalist index described by Esculier et al. (2015). The

119 procedure utilized for this investigation was approved by a university ethical committee (REF

120 637). All runners were free from musculoskeletal pathology at the time of data collection and

- 121 provided written informed consent in accordance with the principles outlined in the Declaration
- 122 of Helsinki.

124 *Footwear*

The footwear used during this study consisted of New Balance, 1260 v2 (New Balance, Boston, Massachusetts, United States; henceforth termed conventional) and Vibram Five-Fingers, ELX (Vibram, Albizzate, Italy; henceforth termed minimal) (Figure 1). The conventional footwear had an average mass of 0.285 kg, heel thickness of 25 mm and a heel drop of 14 mm and minimal an average mass of 0.167 kg, heel thickness of 7 mm and a heel drop of 0 mm. The footwear were also scored using the minimalist index of Esculier et al. (2015), and the conventional footwear received a score of 20 and minimal a score of 92.

- 132
- 133

@@@FIGURE 1 NEAR HERE@@@

134

135 *Procedure*

Participants ran at 4.0 m/s (\pm 5%), striking an embedded piezoelectric force platform (Kistler 136 Instruments Ltd., Winterthur, Switzerland) with their right (dominant) foot. Running velocity 137 was monitored using infrared timing gates (Newtest, Oy Koulukatu, Finland). The stance phase 138 was delineated as the duration over which 20 N or greater of vertical ground reaction force 139 140 (GRF) was applied to the force platform. Runners completed five successful trials in each footwear condition. The order that participants ran in each footwear condition was 141 counterbalanced. Kinematic and GRF data were synchronously collected. Kinematic data were 142 captured at 250 Hz via an eight-camera motion analysis system (Qualisys Medical AB, 143 Goteburg, Sweden). Dynamic calibration of the motion capture system was performed before 144 each data collection session. 145

Body segments were modelled in 6 degrees of freedom using the calibrated anatomical systems 147 technique (Cappozzo et al. 1995). To define the anatomical frames of the thorax, pelvis, thighs, 148 shanks and feet retroreflective markers were placed at the C7, T12 and xiphoid process 149 landmarks and also positioned bilaterally onto the acromion process, iliac crest, anterior 150 superior iliac spine (ASIS), posterior super iliac spine (PSIS), medial and lateral malleoli, 151 medial and lateral femoral epicondyles, greater trochanter, calcaneus, first metatarsal and fifth 152 153 metatarsal. Carbon-fibre tracking clusters comprising of four non-linear retroreflective markers were positioned onto the thigh and shank segments. In addition to these, the foot segments were 154 155 tracked via the calcaneus, first metatarsal and fifth metatarsal, the pelvic segment was tracked using the PSIS and ASIS markers and the thorax segment was tracked using the T12, C7 and 156 xiphoid markers. Static calibration trials were obtained in each footwear allowing for the 157 anatomical markers to be referenced in relation to the tracking markers/ clusters. 158

159

To measure axially directed accelerations at the tibia, an accelerometer (Biometrics ACL 300, Gwent United Kingdom) sampling at 1000Hz was used. The device was mounted onto a piece of lightweight carbon-fibre material using the protocol outlined by Sinclair et al. (2013a). The accelerometer was attached securely to the distal anterio-medial aspect of the tibia in alignment with its longitudinal axis, 0.08 m above the medial malleolus. Strong non-stretch adhesive tape was placed over the device and leg to avoid overestimating the acceleration due to tissue artefact (Sinclair et al. 2013a).

167

168 *Processing*

Dynamic trials were digitized using Qualisys Track Manager (Qualisys Medical AB, Goteburg,
Sweden) in order to identify anatomical and tracking markers then exported as C3D files to
Visual 3D (C-Motion, Germantown, MD, USA). All data were linearly normalized to 100 %

of the stance phase. GRF data and marker trajectories were smoothed with cut-off frequencies 172 of 50 Hz at 12 Hz respectively, using a low-pass Butterworth 4th order zero lag filter. In 173 addition, the tibial acceleration signal was filtered using a 60 Hz Butterworth zero lag 4th order 174 low pass filter (Sinclair et al. 2013a). Kinematics of the hip, knee and ankle were quantified 175 using an XYZ cardan sequence of rotations (where X is flexion-extension; Y is ab-adduction 176 and is Z is internal-external rotation). In addition, tibial internal rotation kinematics were also 177 178 calculated in accordance with Eslami et al. (2007). All force parameters throughout were normalized by dividing by bodyweight (BW). 179

180

In accordance with the protocol of Addison & Lieberman, (2015), an impulse-momentum modelling approach was utilized to calculate effective mass (% BW), which was quantified in accordance with the below equation:

184

185 Effective mass = vertical GRF integral / (Δ foot vertical velocity + gravity * Δ time)

186

The impact peak was defined firstly in non-habitual runners when wearing conventional 187 footwear, as the first peak in vertical GRF. In habitual runners and non-habitual runners 188 wearing minimal footwear where no impact peak was expected, according to the protocols of 189 Lieberman et al. (2010) and Sinclair et al. (2018a) we defined the position of the impact peak 190 at the same relative position, which was shown to be 11.87 % of the stance phase. The time 191 192 (ms) to impact peak (Δ time) was quantified as the duration from footstrike to impact peak. The vertical GRF integral (BW·ms) during the period of the impact peak was calculated using a 193 trapezoidal function. The change in foot vertical velocity (Δ foot vertical velocity) was 194 determined as the instantaneous vertical foot velocity averaged across the 10 frames prior to 195

- the impact peak (Sinclair et al. 2018a). The velocity of the foot was quantified using the centreof mass of the foot segment in the vertical direction, within Visual 3D (Sinclair et al. 2018a).
- 198

Loading rate (BW/s) was also was also extracted by obtaining the peak increase in vertical 199 200 GRF between adjacent data points using the first derivative function within Visual 3D and the peak tibial acceleration (g) was extracted as the highest positive acceleration peak during the 201 stance phase. The strike index was calculated as the position of the centre of pressure location 202 at footstrike, relative to the total length of the foot (Squadrone et al. 2015). A strike index of 203 0-33% denotes a rearfoot, 34-67% a midfoot and 68-100% a forefoot strike pattern. Finally, 204 limb stiffness during running was quantified using a mathematical spring-mass model 205 (Blickhan, 1989). Limb stiffness (BW/m) was calculated from the ratio of the peak normalized 206 vertical GRF to the maximum vertical compression of the leg spring which was calculated as 207 the change in limb length from footstrike to minimum length during the stance phase (Farley 208 209 & Morgenroth, 1999). Limb length was quantified as the vertical height of the proximal end of the thigh segment within Visual 3D. 210

211

212 Following this, data during the stance phase were exported from Visual 3D into OpenSim 3.3 software (Simtk.org). Two validated musculoskeletal models were used to process the 213 biomechanical data both of which were scaled to account for the anthropometrics of each 214 runner. The first with 12 segments, 19 degrees of freedom and 92 musculotendon actuators 215 (Lerner et al. 2015) was used initially to estimate lower extremity joint forces. As muscle forces 216 are the main determinant of joint compressive forces (Herzog et al. 2003), muscle kinetics were 217 218 quantified using static optimization in accordance with Steele et al. (2012). Compressive patellofemoral, medial/lateral tibiofemoral, ankle and hip joint forces were calculated via the 219

process as inputs. Furthermore, patellofemoral stress (KPa/kg) was quantified by dividing the patellofemoral force by the contact area. Patellofemoral contact areas were obtained by fitting a polynomial curve to the sex specific data of Besier et al. (2005), who estimated patellofemoral contact areas as a function of the knee flexion angle using MRI. Finally, Achilles tendon forces

joint reaction analyses function using the muscle forces generated from the static optimization

were estimated in accordance with the protocol of Almonroeder et al. (2013), by summing the

muscle forces of the medial gastrocnemius, lateral, gastrocnemius, and soleus muscles.

227

220

In addition, patellofemoral, medial/ lateral tibiofemoral, ankle, hip and Achilles tendon instantaneous load rates (BW/s and KPa/BW/s) were also extracted by obtaining the maximum increase in force/ stress between adjacent data points using the first derivative function in Visual 3D. Finally, the integral of the hip, tibiofemoral, ankle, patellofemoral and Achilles tendon forces (BW·s) and stresses (KPa/BW·s) during the stance phase were calculated using a trapezoidal function.

234

Running in minimal footwear has been shown to alter step length during running, which increases the number of footstrikes necessary to run a set distance. We therefore estimated the total impulse per kilometre ($\mathbf{BW} \cdot \mathbf{km}$) by multiplying these parameters by the number of steps required to run a **kilometre**. The number of steps required to complete one **kilometre** was quantified using the step length (m), which was determined by taking the difference in the horizontal position of the foot centre of mass between the right and left legs at footstrike.

241

The second model also had twelve segments, 23 degrees of freedom and 92 muscle-tendon actuators and was adapted from the generic OpenSim gait2392 model to include the iliotibial band (Foch et al. 2013). The iliotibial band itself was included within the gait2392 model but

as a muscle with only a passive contractile component and an optimal muscle fiber length of 245 zero (Foch et al. 2013). Iliotibial band kinematics during the stance phase were calculated via 246 the muscle analyses function within OpenSim and iliotibial band strain (%) was calculated by 247 dividing the change in length of the band during stance and dividing by its resting length at each 248 time frame. In addition, the strain rate (%/s) was calculated as the change in strain between 249 adjacent data points. The resting length of the iliotibial band was determined as its length during 250 251 the static calibration trial (Hamill et al. 2008). Peak iliotibial band strain and strain rate were measured at the instance of peak knee flexion during stance (Hamill et al. 2008). 252

253

254 *Statistical analyses*

Following data processing, compressive joint forces (hip, patellofemoral, medial tibiofemoral) 255 and lateral tibiofemoral), Achilles tendon loading and three-dimensional kinematics during the 256 entire stance phase were temporally normalized using linear interpolation to 101 data points. 257 Differences across the entire stance phase were examined using 1-dimensional statistical 258 parametric mapping (SPM) with MATLAB 2017a (MATLAB, MathWorks, Natick, USA), in 259 accordance with Pataky et al. (2016), using the 260 source code available at http://www.spm1d.org/. Differences as a function of both FOOTWEAR (FOOTWEAR -261 conventional or minimal) and GROUP (GROUP - habitual or non-habitual) were examined 262 using paired and independent t-tests (SPM t). 263

264

For discrete parameters that could not be examined using SPM (joint integral, joint loading rate, joint integral per kilometre, step length, instantaneous load rate, strike index, limb stiffness, tibial accelerations, iliotibial band strain, iliotibial band strain rate and effective mass), means and standard deviations were calculated for each condition. Differences in discrete biomechanical parameters were examined using 2 (FOOTWEAR – conventional of

270	minimal) x 2 (GROUP- habitual or non-habitual) mixed ANOVAs, Effect sizes were calculated
271	using partial eta ² ($p\eta^2$). In the event of a significant interaction, simple main effects tests were
272	adopted. Discrete statistical actions were conducted using SPSS v25.0 (SPSS Inc., Chicago,
273	USA). Statistical significance was accepted at the P≤0.05 level.
274	
275	Results
276	@@@TABLE 1 NEAR HERE@@@
277	@@@TABLE 2 NEAR HERE@@@
278	
279	Lower extremity external loading, strike index and step length
280	For effective mass there was a significant FOOTWEAR*GROUP interaction (P=0.01, $p\eta^2$ =
281	0.31). Simple main effects tests showed that effective mass was larger in the conventional
282	running shoes compared to minimal in habitual runners (P=0.01, $p\eta^2 = 0.53$) but there were no
283	significant differences between footwear in non-habitual runners (P=0.26, $p\eta^2 = 0.11$). In
284	addition, when wearing minimal footwear, effective mass was significantly greater in non-
285	habitual runners compared to habitual (P<0.001, $p\eta^2 = 0.61$) but there were no differences
286	between habitual and non-habitual runners when running in conventional footwear (P=0.50,
287	$p\eta^2 = 0.03$) (Table 1).
288	
289	For loading rate there was also a significant FOOTWEAR*GROUP interaction (P=0.002, pq ²
290	= 0.41). Simple main effects tests showed that loading rate was significantly larger in the
291	minimal footwear compared to conventional in non-habitual runners (P=0.004, $p\eta^2 = 0.63$) but
292	there was no significant difference between footwear in habitual runners (P=0.94, $p\eta^2 < 0.001$).
293	In addition, when wearing minimal footwear, the loading rate was significantly greater in non-

295	running in conventional footwear (P=0.06, $p\eta^2 = 0.19$) (Table 1).
296	
297	For peak tibial accelerations, there was a significant FOOTWEAR*GROUP interaction
298	(P=0.005, $p\eta^2 = 0.36$). Simple main effects tests showed that tibial accelerations were
299	significantly larger in minimal footwear compared to conventional in non-habitual runners
300	(P=0.03, $p\eta^2 = 0.42$) but there was no significant difference between fotowear in habitual
301	runners (P=0.09, $p\eta^2$ =0.29). In addition, when wearing minimal footwear, tibial accelerations
302	were significantly greater in non-habitual compared to habitual runners (P<0.001, $p\eta^2 = 0.57$)
303	but there were no differences between habitual and non-habitual runners in conventional
304	footwear (P=0.20, $p\eta^2 = 0.09$) (Table 1).
305	
306	For limb stiffness there was a significant FOOTWEAR*GROUP interaction (P=0.04, $p\eta^2$ =
307	0.21). Simple main effects tests showed that limb stiffness was greater in minimal compared to
308	conventional footwear in non-habitual runners (P<0.001, $p\eta^2 = 0.57$) but there were no
309	differences between footwear when running in conventional footwear (P=0.20, $p\eta^2 = 0.09$)
310	(Table 1).
311	
312	For strike index there was a main effect of FOOTWEAR (P=0.002, $p\eta^2 = 0.36$), which showed
313	that the strike position was more anterior in minimal footwear. In addition, there was also a
314	main effect of GROUP (P=0.007, $p\eta^2 = 0.34$), which indicated that the strike was also more
315	anterior in habitual runners (Table 1).
316	
317	For step length there was a significant FOOTWEAR*GROUP interaction (P=0.04, $p\eta^2 = 0.20$).
318	Simple main effects tests showed that step length was significantly larger in conventional

habitual runners compared to habitual (P<0.001, $p\eta^2 = 0.52$) but there were no differences when

319	compared to minimal footwear in habitual runners (P=0.001, $p\eta^2 = 0.72$) but there was no
320	difference between footwear in non-habitual runners (P=0.70, $p\eta^2 = 0.02$). In addition, when
321	wearing minimal footwear compared to conventional, step length was significantly greater in
322	non-habitual runners (P=0.02, $p\eta^2 = 0.28$) but there were no differences between habitual and
323	non-habitual runners when running in conventional footwear (P=0.11, $p\eta^2 = 0.14$) (Table 1).
324	
325	Joint loading
326	For medial tibiofemoral loading rate there was a significant FOOTWEAR*GROUP interaction
327	(P<0.001, $p\eta^2 = 0.76$). Simple main effects tests showed that the loading rate was significantly
328	larger in the conventional compared to minimal footwear in habitual runners (P=0.001, $p\eta^2$ =
329	0.91) but significantly greater in minimal compared to conventional footwear in non-habitual
330	runners (P=0.005, $p\eta^2 = 0.61$). In addition, when wearing minimal footwear, medial
331	tibiofemoral loading rate was significantly greater in non-habitual compared to habitual runners
332	(P=0.02, $p\eta^2 = 0.26$) but in conventional footwear was significantly greater in habitual
333	compared to non-habitual runners (P=0.04, $p\eta^2 = 0.21$) (Table 1).
224	
334	
335	For the integral of patellofemoral joint force, there was a main effect of FOOTWEAR (P=0.03,

336 $p\eta^2 = 0.25$), which was shown to be larger in conventional footwear (Table 1).

337

For the integral of Achilles tendon force, there was a main effect of FOOTWEAR (P=0.02, $p\eta^2$ = 0.27), which was shown to be larger in minimal footwear. In addition, there was a main effect for GROUP (P=0.002, $p\eta^2$ =0.42), which indicated that the Achilles tendon integral was greater in habitual runners (Table 1). For the Achilles tendon integral per kilometre, there was a main

342	effect of FOOTWEAR (P=0.004, $p\eta^2 = 0.38$), which was shown to be larger in minimal
343	footwear. In addition, there was a main effect for GROUP (P=0.002, $p\eta^2 = 0.41$), which
344	indicated that the Achilles tendon integral was greater in habitual runners (Table 2).
345	
346	For the ankle integral per kilometre, there was a main effect for GROUP (P=0.02, $p\eta^2 = 0.27$),
347	which indicated that the ankle integral was greater in habitual runners (Table 2).
348	
349	Iliotibial band kinematics
350	For iliotibial band strain rate, there was a main effect for GROUP (P<0.001, $p\eta^2 = 0.52$), which
351	indicated that the strain rate was greater in non-habitual runners (Table 1).
352	
353	Statistical parametric mapping - joint loading
354	Minimal footwear was associated with increased Achilles tendon force compared to
355	conventional running shoes in the first 20% of the stance phase in both habitual and non-
356	habitual runners (Figure 2ab).
357	
358	Statistical parametric mapping - three-dimensional kinematics
359	Conventional footwear was associated with increased hip flexion compared to minimal from
360	20-40% of the stance phase in habitual runners (Figure 2c). Conventional footwear was also
361	associated with increased knee flexion compared to minimal from 40-60% of the stance phase
362	in both habitual and non-habitual runners (Figure 2de). In additional, minimal footwear

363 compared to conventional was associated with increased tibial and knee internal rotation during
364 from 20-60% of the stance phase in habitual runners (Figure 3ab). Furthermore, it was revealed
365 that the ankle exhibited increased plantarflexion in minimal footwear from 0-5% of the stance
366 phase in both habitual and non-habitual runners (Figure 3cd). Finally, in conventional footwear
367 compared to minimal, habitual runners were similarly associated with increased plantarflexion
368 from 0-5% of the stance phase (Figure 3e).

- 369
- 370@ @ @ FIGURE 2 NEAR HERE@ @ @
 - @@@FIGURE 3 NEAR HERE@@@

372

371

373 Discussion

The aim of the current investigation was to examine differences in running biomechanics between minimal and conventional footwear, in those who habitually wear minimal and conventional footwear. To the authors knowledge, this is the first quantitative comparison of these footwear in habitual and non-habitual minimal footwear users using a musculoskeletal simulation and SPM based approach.

379

380 The kinematic analysis using SPM of the sagittal plane ankle angle aligned with the discrete analysis of the strike index, supports previous investigations in that minimal footwear 381 transferred the footstrike to a more anterior position in both habitual and non-habitual runners 382 383 (Squadrone et al. 2015; Sinclair et al. 2019). Furthermore, in support of previous analyses the findings from this study also showed that habitual minimal footwear users similarly were 384 associated with a significantly more anterior footsrike position in relation to non-habitual 385 runners (Larson et al. 2014). It is important to contextualize the strike index values observed in 386 both conditions, as regardless of which footwear condition was utilized non-habitual runners 387

maintained a rearfoot strike pattern and habitual runners adopted a midfoot contact position.
This supports proposition of Tam et al. (2017) that in acute investigations non-habitual runners
do not sufficiently alter their running mechanics and continue to exhibit a rearfoot strike pattern.

For the indices of external loading, in agreement with previous analyses this investigation 392 showed that tibial accelerations and loading rates were found to be greater in minimal footwear 393 394 in non-habitual runners (Sinclair et al. 2013ab) and in non-habitual runners when wearing minimal footwear (Lieberman et al. 2010). As non-habitual runners adopted a rearfoot strike 395 396 pattern when wearing minimal footwear, it was expected that both effective mass and limb stiffness were also increased when non-habitual runners adopted minimal footwear. It is 397 proposed that the increases in external loading indices were mediated by the corresponding 398 399 changes in effective mass and limb stiffness, which have been shown previously to be positively 400 related to the magnitude of the both tibial accelerations and loading rate (Sinclair et al. 2018a). As tibial accelerations/ loading rates were increased in non-habitual runners using minimal 401 402 footwear, these observations may be clinically meaningful. Given the proposed association between tibial accelerations/ loading rates and the aetiology of chronic injuries (Davis et al. 403 2004), this study indicates that non-habitual runners wearing minimal footwear are at increased 404 risk from impact related injuries. 405

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Although no differences were revealed using SPM, the discrete analysis showed that the patellofemoral force integral was significantly larger in conventional footwear in both habitual and non-habitual groups. This finding concurs with those observed previously by Sinclair, (2014), Sinclair et al. (2016) and Bonacci et al. (2014) who showed significant reductions in patellofemoral loading when running in minimal footwear. The discrete and SPM based analyses showed that minimal footwear transferred the footstrike to a more anterior position

and also reduced the extent of peak knee flexion in both habitual and non-habitual groups. It 413 is proposed that these observations are responsible for the reductions in patellofemoral loading 414 415 as previous analyses have shown that the function of the knee joint as an energy absorber is reduced when there is an increased plantarflexion involvement (Sinclair & Selfe, 2015). 416 Importantly, excessive patellofemoral joint loading is considered a key mechanism linked to 417 the aetiology of pain symptoms in active individuals (Ho et al. 2012). Therefore, the findings 418 419 from the current investigation indicate that in both habitual and non-habitual runners, minimal footwear may be effective in attenuating the biomechanical parameters linked to the aetiology 420 421 of patellofemoral pain.

422

423 In addition, it was revealed via the discrete analysis, that the loading rate at the medial aspect of the tibiofemoral joint was larger in the conventional footwear in habitual runners and in 424 minimal footwear in non-habitual runners. This supports those of Sinclair et al. (2018b) who 425 showed in non-habitual runners, that minimal footwear increased the loading rate at the medial 426 aspect of the knee joint. This observation indicates that the loading rate at the medial 427 tibiofemoral joint was statistically larger when runners performed in their non-preferred 428 footwear condition. Because the loading rate at the medial knee has been cited as important 429 predictor of radiographic knee osteoarthritis, the findings from this investigation indicate that 430 runners are at increased risk when running in their non-preferred footwear condition without 431 habituation (Morgenroth et al. 2014). 432

433

Furthermore, this investigation showed using both SPM and discrete analyses that Achilles tendon loading indices were significantly larger in minimal footwear and in habitual runners collectively. This observation concurs with previous investigations (Sinclair, 2014, Sinclair et al. 2019) showing that in non-habitual runners' minimal footwear significantly enhanced

Achilles tendon loading compared to conventional running shoes, although there is no 438 comparative literature examining the mechanics of the Achilles tendon in habitual minimal 439 footwear users. Importantly, the current study also showed that habitual runners were associated 440 with enhanced Achilles tendon loading compared to non-habitual users. It is proposed that the 441 mechanism responsible for these observations is the more anterior footsrike position in minimal 442 footwear and in habitual users, which served to enhance triceps surae muscle forces during the 443 eccentric aspect of the stance phase (Almonroeder et al. 2013). This observation may be 444 clinically important, as the initiation of Achilles tendinopathy is believed to be mediated 445 446 through repeated and excessive loads experienced by tendon itself without sufficient rest in between loading exposures (Selvanetti et al. 1997). However, Davis et al. (2017) postulate that 447 greater tendon loading in habituated runners may instigate the stimulus required for tendon 448 hypertrophy and enhanced stiffness within the muscle-tendon unit necessary for the storage 449 and release of elastic energy. Anrsten et al. (2017) support this notion as they showed that 450 habitual minimal footwear users were associated with greater tendon cross sectional area and 451 increased stiffness. 452 453

Finally, the current study also importantly showed that iliotibial band strain rate was greater in 454 non-habitual runners. This finding may be clinically important as modelling investigations 455 suggest that increased strain rate is the biomechanical risk factor linked to the aetiology of 456 iliotibial band syndrome (Hamill et al. 2008). The main mechanical difference (irrespective of 457 footwear) between groups, was the adoption of a midfoot strike pattern in habitual minimal 458 footwear users compared to non-habitual. Therefore, the findings from this study lend support 459 to the proposition of Lalonde (2013) that a rearfoot landing should be avoided for the 460 prevention of iliotibial band syndrome in runners, although further aetiological investigations 461 are required to substantiate this notion. As such, the current investigation indicates that 462

transitioning to minimal footwear may be beneficial for runners in that they are able to attenuatetheir risk from iliotibial band syndrome.

465

A potential limitation to the current study that should be acknowledged is that only male runners 466 were examined. Females have been shown to exhibit distinct external loading kinetics (Ferber 467 et al. 2003), lower extremity kinematics (Sinclair et al. 2012, Ferber et al. 2003), limb stiffness 468 (Sinclair et al. 2016), patellofemoral (Sinclair & Selfe, 2015) and Achilles tendon (Greenhalgh 469 & Sinclair, 2014), parameters compared to male runners. This therefore suggests that further 470 investigation of minimal footwear in habitual users using a female sample is warranted before 471 472 comprehensive conclusions can be drawn. Furthermore, the efficacy of musculoskeletal simulation analyses depends on the fidelity of the primary neuromusculoskeletal model used to 473 quantify the mechanics of the movement being investigated (Seth et al., 2011). Many 474 assumptions and simplifications are made in the development of musculoskeletal simulation 475 models, which could potentially impact the results from the current investigation (Seth et al., 476 2011). Therefore, there is considerable scope for future analyses to address and improve upon 477 these limitations, in order to provide more accurate and valid musculoskeletal simulations. 478

479

480 In conclusion, the biomechanics of minimal and conventional footwear have received widespread research attention. However, there has not been quantitative comparison of these 481 footwear in habitual and non-habitual minimal footwear users using a musculoskeletal 482 483 simulation and SPM based approach. This study revealed that minimal footwear mediated a more anterior contact position in both groups, although non-habitual runners still adopted a 484 rearfoot strike pattern. In addition, minimal footwear increased tibial accelerations, loading 485 rates and medial tibiofemoral loading rates in non-habitual runners and decreased 486 patellofemoral loading in both habitual and non-habitual groups. Finally, Achilles tendon 487

loading indices were larger in minimal footwear and in habitual runners whereas iliotibial band strain rate was reduced in habitual runners. Therefore, this study highlights firstly the importance of transitioning to minimal footwear and also indicates that post transition they may be effective in attenuating the biomechanical mechanisms linked to the aetiology of many chronic injuries.

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Table 1: Discrete biomechanical parameters (mean \pm standard deviations) as a function of FOOTWEAR

and GROUP.

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	Non-habitual					Hab	Habitual		
	Conver	ntional	Min	imal	Conve	ntional	Min	imal	
	Mean	SD	Mean	SD	Mean	SD	Mean	SD	
Effective mass (% BW)	9.59	1.93	11.32	1.81	9.06	1.53	7.83	1.01	B, C
Loading rate (BW/s)	154.36	69.86	293.00	126.14	105.97	27.20	105.44	48.95	A, B, C
Peak tibial acceleration (g)	8.16	2.04	9.54	1.90	7.06	1.60	6.35	0.86	B, C
Limb stiffness (BW/m)	63.41	28.52	65.91	22.69	63.46	33.51	48.12	13.97	С
Iliotibial band strain (%)	2.41	2.09	2.44	1.85	2.09	2.18	2.54	1.27	
Iliotibial band strain rate (%/s)	42.87	14.67	42.96	12.71	30.30	7.37	28.32	8.06	В
Patellofemoral integral (BW·s)	0.29	0.08	0.26	0.08	0.31	0.13	0.28	0.10	А
Patellofemoral loading rate (BW/s)	156.50	55.49	154.50	33.75	179.18	48.37	143.14	22.99	
Patellofemoral stress integral (KPa/BW·s)	0.56	0.14	0.52	0.13	0.59	0.21	0.55	0.18	
Patellofemoral stress loading rate (KPa/BW/s)	323.28	125.29	326.40	81.24	375.92	117.61	302.65	59.30	
Achilles integral (BW·s)	0.65	0.07	0.71	0.05	0.71	0.05	0.79	0.12	A, B
Achilles loading rate (BW/s)	153.96	43.34	179.34	67.96	179.34	67.96	148.14	38.75	
Ankle integral (BW·s)	1.21	0.12	1.30	0.12	1.30	0.12	1.33	0.19	
Ankle loading rate (BW/s)	251.82	41.42	281.18	55.95	281.18	55.95	247.14	40.27	
Hip integral (BW·s)	1.34	0.16	1.31	0.09	1.31	0.09	1.25	0.13	
Hip loading rate (BW/s)	276.22	41.21	291.88	82.86	291.88	82.86	260.00	123.79	
Medial tibiofemoral integral (BW·s)	0.86	0.10	0.83	0.06	0.83	0.06	0.85	0.12	
Medial tibiofemoral loading rate (BW/s)	212.57	51.75	274.96	75.23	274.96	75.23	196.17	64.60	С
Lateral tibiofemoral integral (BW·s)	0.44	0.07	0.44	0.05	0.44	0.05	0.41	0.07	
Lateral tibiofemoral loading rate (BW/s)	157.20	63.56	151.07	38.23	151.07	38.23	130.20	36.26	
Strike index (%) 637 A = main effect of FOOTWEAR	22.61	17.92	33.79	24.69	46.48	21.44	61.68	19.33	A, B

B = main effect of GROUP

639 C = FOOTWEAR x GROUP interaction

Table 2: Discrete temporal biomechanical parameters (mean ± standard deviations) as a function of FOOTWEAR and GROUP.

	Non-habitual				Habitual				
	Conventional		Minimal		Conventional		Minimal		
	Mean	SD	Mean	SD	Mean	SD	Mean	SD	
Step length (m)	1.41	0.14	1.4	0.15	1.29	0.17	1.23	0.15	A, B, C
Patellofemoral integral per kilometre m (BW·km)	543.91	163.20	493.74	160.51	646.21	300.30	612.77	253.39	
Patellofemoral stress integral per kilometre (KPa/BW·km)	1048.04	280.21	970.31	268.78	1203.71	494.77	1188.42	439.10	
Achilles integral per kilometre (BW·km)	1196.94	174.21	1328.26	134.48	1446.36	181.08	1697.98	361.64	A, B
Ankle integral per kilometre (BW·km)	2255.40	334.19	2410.35	249.97	2637.91	428.70	2849.76	582.01	В
Hip integral per kilometre (BW·km)	2507.87	504.79	2465.54	403.70	2672.95	391.66	2676.06	452.34	
Medial tibiofemoral integral per kilometre (BW·km)	1608.00	298.37	1561.71	234.69	1694.68	239.98	1826.23	378.21	
Lateral tibiofemoral integral per kilometre (BW·km)	815.75	191.45	826.17	133.47	902.91	173.35	875.81	201.87	
650 A - main affect of EOOTWEAP									

A = main effect of FOOTWEAR 651 652

B = main effect of GROUP

C = FOOTWEAR x GROUP interaction

668 Figure labels



Figure 1: Experimental footwear (A = conventional and B = minimal).



Figure 2: Statistical parametric mapping results of Achilles tendon and ankle forces in addition
to hip and knee kinematics (FOOTWEAR: black = conventional/ red = minimal & GROUP:
black = non-habitual/ red = habitual).



Figure 3: Statistical parametric mapping results of tibial internal rotation, knee and ankle
kinematics (FOOTWEAR: black = conventional/ red = minimal & GROUP: black = nonhabitual/ red = habitual).