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Title	An inductive force sensor for in-shoe plantar normal and shear load measurement
Type	Article
URL	<a href="https://clock.uclan.ac.uk/id/eprint/33839/">https://clock.uclan.ac.uk/id/eprint/33839/</a>
DOI	<a href="https://doi.org/10.1109/JSEN.2020.3006316">https://doi.org/10.1109/JSEN.2020.3006316</a>
Date	2020
Citation	Wang, L, Jones, D, Chapman, Graham, Siddle, H, Russel, D, Alazmani, A and Culmer, P (2020) An inductive force sensor for in-shoe plantar normal and shear load measurement. IEEE Sensors Journal, 20 (22). pp. 13318-13331. ISSN 1530-437X
Creators	Wang, L, Jones, D, Chapman, Graham, Siddle, H, Russel, D, Alazmani, A and Culmer, P

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<https://doi.org/10.1109/JSEN.2020.3006316>

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# An Inductive Force Sensor for In-Shoe Plantar Normal and Shear Load Measurement

Lefan Wang, Dominic Jones, Graham J Chapman, Heidi J Siddle, David A Russell, Ali Alazmani, and Peter Culmer

**Abstract**—Diabetic foot ulcers (DFUs) are a severe global public health issue. Plantar normal and shear load are believed to play an important role in the development of foot ulcers and could be a valuable indicator to improve assessment of DFUs. However, despite their promise, plantar load measurements currently have limited clinical application, primarily due to the lack of reliable measurement techniques particularly for shear load measurements. In this paper we report on the design and evaluation of a novel tri-axis force sensor to measure both normal and shear load on the foot's plantar surface simultaneously. The sensor consists of a group of inductive sensing coils above which a conductive target is placed on a hyperelastic elastomer. Movement of the target under load affects the coil inductances which are measured and digitized by an embedded system. Using a computational finite element model, we investigated the influence of sensing coil form and configuration on sensor performance. A sensor configured with four-square coils and maximal turns provided the best performance for plantar load measurements. A prototype was fabricated and calibrated using a neural network to map the non-linear relationship between the sensor output and the applied tri-axis load. Experimental evaluation indicates that the tri-axis sensor can effectively detect shear load of  $\pm 16$  N and normal load up to 105 N (RMS errors: 1.05 N and 1.73 N respectively) with a high performance. Overall, this sensor provides a promising basis for plantar normal and shear load measurement which are crucial for improved assessment of DFU.

**Index Terms**—Diabetic foot ulcer, Finite element modelling, Neural network, Plantar normal and shear load, Tri-axis force sensor.

## I. INTRODUCTION

**D**IABETES is a major public health concern. Worldwide, 415 million people are living with diabetes, with estimates rising to 642 million (10% of world population) by 2040 [1]. Foot ulceration is a common and devastating complication of diabetes. It can lead to infection, amputation, and even death if timely interventions are not performed, with an approximate 40% mortality at 5 years in patients with diabetes who underwent amputation [2]. Additionally,

diabetic foot ulcers (DFUs) cause a substantial economic and social burden, with NHS England spending approximately £1.13 billion on treatment of DFUs in 2014-15 [3], [4]. This figure is expected to rise to £2.1 billion by 2035/6 [3]. In the US, the annual medical cost for the management of diabetic foot ranges from \$9-13 billion.

Elevated or abnormal plantar pressure (the pressure on the sole of the foot) is commonly considered as a major causative factor in the development of DFUs [5]–[8]. However, recent studies indicate that the importance of plantar shear stresses in predication of ulcer formation have been underestimated [9] and that utilizing both pressure and shear stress provides a more effective means to identify and assess abnormal pressure loads associated with DFUs [10]. Measurement of shear stresses is a significant challenge, predominantly due to the conformable nature of the foot's plantar surface and the high load ranges experienced (generally up to 740 kPa (peak pressure) and 140 kPa (peak shear)) [9], [11]–[14].

A variety of commercial systems has been developed to measure plantar loading, including sensing platforms and wearable sensory insoles. Notable examples include Pedar<sup>®</sup> [15], F-Scan<sup>™</sup> [16], medilogic WLAN insole [17], BioFoot<sup>®</sup> [18], P-WALK [19], emed<sup>®</sup> [20], MatSCAN<sup>™</sup> [21], and footscan<sup>®</sup> [22]. These systems share a common measurement limitation of solely measuring plantar pressure, without the capability of measuring shear stress. The strain gauge based Cleveland Clinic Plate [9], [23] and the camera-based Foot-STEPS platform [24] are reported to measure both plantar pressure and shear stress, but they are non-portable, only allowing static and limited dynamic measurements of 1-2 stance phases.

Researchers have attempted to address this situation through a variety of multi-axis sensing modalities including capacitive, resistive, piezoelectric and inductive systems [25]. Multi-axis (typically tri-axis) capacitive sensors generally embed four capacitive elements which can be used to obtain pressure and shear stress through selective decoupling of the output signals. In 2008, Lee *et al.* [26] reported a  $8 \times 8$  tri-axis sensing array, each sensor node with a full-scale range of 131 kPa in three directions. In 2015, Liang *et al.* [27] implemented a  $4 \times 4$  sensing array in which each sensor unit has a dimension of  $4.0 \text{ mm} \times 4.0 \text{ mm} \times 1.1 \text{ mm}$  and provides a measurement range of 31 kPa and 250 kPa for shear stress and pressure, respectively. Inductive sensors have received increasing attention for monitoring plantar load due to robustness of environmental factors. In 2012, Wattanasarn *et al.* [28] designed a 3D flexible force sensor consisting of a detection coil layer and an excitation coil layer, each

This work was supported by the UK EPSRC under Grant EP/R041776/1.

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layer with four planar square coils. The design was compact ( $7.2 \text{ mm} \times 7.2 \text{ mm} \times 2.5 \text{ mm}$ ) although sensor performance was limited in measurement range (11.8 kPa, 11.3 kPa, and 15.7 kPa in the x-, y-, and z-axis, respectively). In 2015, Du *et al.* [29] implemented a three-coil inductive sensor, one coil sensitive to pressure and the other two sensitive to both pressure and shear stress. The sensor prototype was used to measure the load distribution under the foot during normal gait but the spatial resolution was limited by the large sensor size ( $76.2 \text{ mm} \times 76.2 \text{ mm} \times 22 \text{ mm}$ ). To the best of the authors' knowledge, a sensor capable of providing high-spatial resolution while obtaining multi-axis measurement of plantar pressure and shear stress is not available.

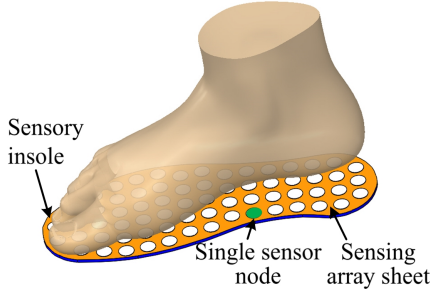


Fig. 1: Illustration of a sensory insole integrated with an array of force sensors for measuring plantar load.

This research aims to develop a tri-axis force sensing unit for measurement of DFU plantar loading, using our previous work in inductive load sensing as a foundation [30], [31]. Our concept is to integrate an array of such sensors within a shoe sole, enabling load mapping across the plantar surface as shown in Fig. 1. This entails optimization of the individual sensing unit to meet the sensing requirements associated with in-shoe measurement of plantar loading in people at risk of diabetic foot ulcers. These aspects are difficult to define due to a lack of appropriate measurement systems and associated plantar loading data. In this context, load requirements have been estimated from pioneering studies using foot force sensing plates capable of shear-load measurement [9], [11]–[14], while sensor size (determining the maximum spatial resolution which can be achieved using a sensing array) is drawn from research-grade in-shoe measurement systems [23], [32]–[34], summarized in Table I.

TABLE I: Sensing requirements for measuring plantar load under diabetic foot.

Measuring capability [9], [11]–[14]	Pressure $\geq 740 \text{ kPa}$
	Shear stress $\geq 140 \text{ kPa}$
Recommended measurement surface/spatial resolution [23], [32]–[34]	$\leq 15 \text{ mm} \times 15 \text{ mm}$
Sampling rate [35], [36]	$\geq 50 \text{ Hz}$

Here we report on optimization and evaluation of the tri-axis sensing element for simultaneous measurement of plantar normal and shear load. This represents the first sensor optimized to measure these quantities, engineered to meet a series of clinically-informed requirements listed in Table I. Section II

provides an overview of the operating principles then Section III investigates optimization of the inductive coil configuration. This is used as the basis for fabrication of a prototype, reported in Section IV together with methods for calibration and multi-axis experimental evaluation.

## II. PRINCIPLE OF OPERATION

Sensors using the principle of eddy-current formation are widely used, particularly in non-contact displacement sensing applications. Generally, an eddy-current displacement sensor comprises a sensing coil and a conductor. As an alternating current flows through the coil, a magnetic field is generated surrounding it. If the conductor is brought into the vicinity of the coil, eddy currents will be induced on the conductor's surface. According to Lenz's law, the eddy current creates its own magnetic field that opposes the original field generated by the coil. The coupling between the coil and the conductor causes variations in their inductance and resistance.

A force sensor can be adapted from eddy-current based displacement sensors by adding an elastic medium between the coil and the conductor. As illustrated in Fig. 2(a), when an external force is applied, the elastomer deforms and accordingly the displacement of the conductor (target) changes, thus altering the coil inductance. Provided the conductor has sufficient thickness, it also acts to mask effect of external conductors (e.g. the foot in this application [31]). Recent developments in inductance digitizing integrated circuits (LDCs) [37] enable fast, accurate measurement of this inductance which can then be mapped to applied force. LDCs detect coil inductance by measuring the oscillation frequency of L-C resonators. As shown in Fig. 2(b), a single coil can be modeled by a RLC parallel electrical model, and it forms an L-C resonant oscillator by connecting the coil with an external capacitor  $C_{ext}$ . The oscillation frequency varies with the sensor inductance. Once the oscillation frequency is measured by LDCs, the coil inductance can be derived using the following equation.

$$L = \frac{1}{(2\pi f)^2(C_{para} + C_{ext})} \quad (1)$$

where  $f$  is the oscillation frequency of the L-C network,  $C_{para}$  is the parasitic capacitance of the coil, and  $C_{ext}$  is an external capacitor.  $C_{para}$  is typically a few picofarads for planar coils of this size [38]–[40] and can thus be neglected as  $C_{ext} \gg C_{para}$ .

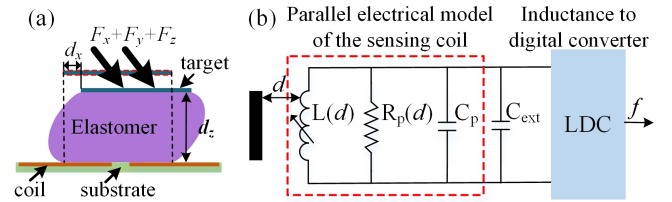


Fig. 2: (a) Illustration of an eddy-current-based tri-axis force sensor, (b) the inductance measurement for a single sensing coil.

Based on this basic transducer mechanism, researchers have proposed and developed tri-axis inductive sensors for various

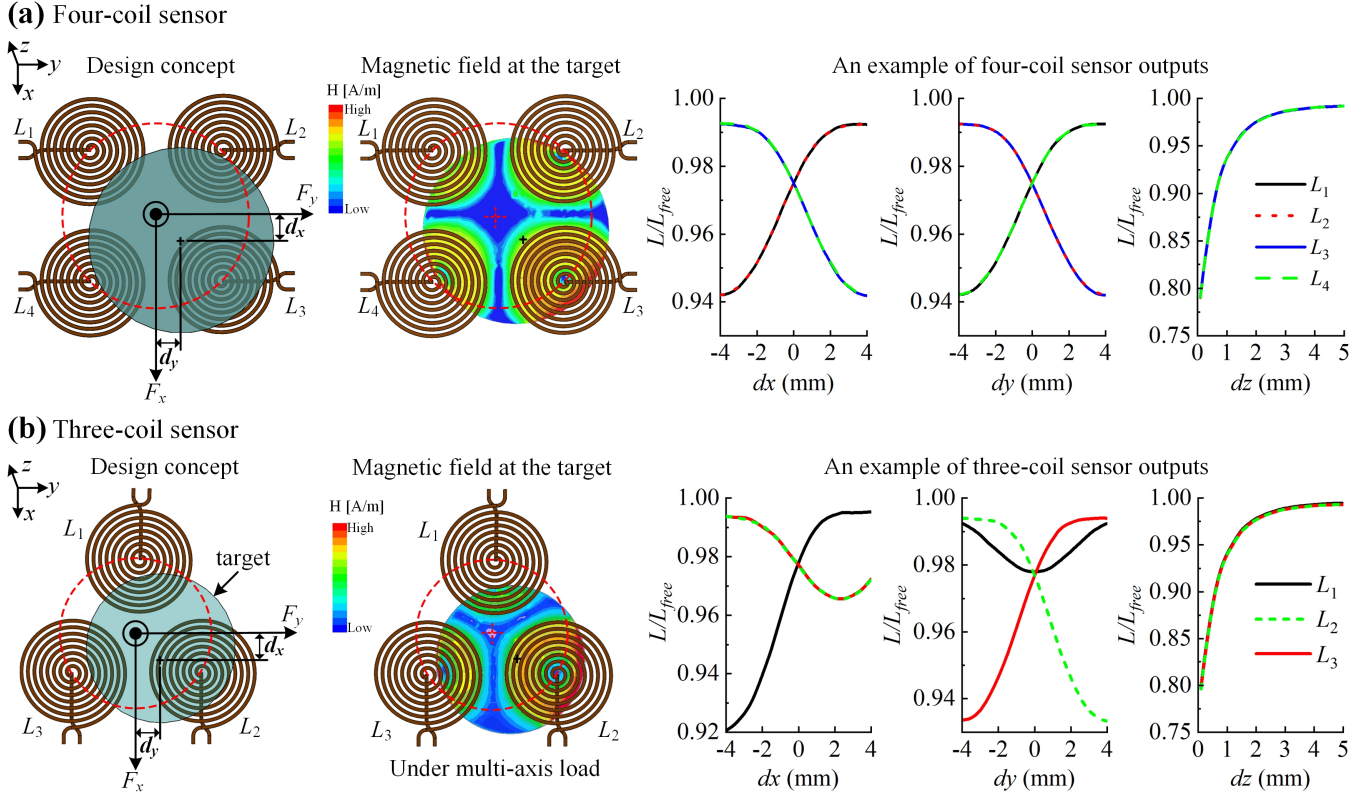


Fig. 3: Schematic, operating principle and representative response of tri-axis inductive force sensors with different configurations; (a) sensor consisting of four symmetric sensing coils; (b) sensor consisting of three coils,  $L_i$  represents the inductance of coil  $i$  ( $i = 1, 2, 3, 4$ ).

multi-axis force measurement applications [28], [29], [31], [41], [42]. In general, the sensor requires one inductive coil per independent measurement axis. For tri-axis sensors, both three and four coils are common, where a four-coil arrangement brings the advantage of an axially symmetric structure. Fig. 3 illustrates their respective operating behavior with simulated responses from the coils generated using a computational simulation described in Section III. For the four-coil sensor, shown in Fig. 3(a), application of a perpendicular force ( $F_z$ ) moves the target closer to all coils, increasing the magnetic coupling and thus the coil inductances ( $L_1 - L_4$ ) will decrease. Applying a shear load ( $F_x$ ) the magnetic coupling with coils 1 and 2 decreases whilst the coupling with coils 3 and 4 increases. This causes a corresponding increase in  $L_1$  and  $L_2$  and decrease in  $L_3$  and  $L_4$ . The same principle applies to loading along the y-axis. The three-coil arrangement, follows the same mechanisms but differs with a more complex response to shear loading due to its asymmetric coil arrangement, as shown in Fig. 3(b). In both configurations, the relationship between the applied load and coil inductances is coupled and non-linear. Thus to obtain the components of applied force ( $F_x$ ,  $F_y$ , and  $F_z$ ) requires appropriate decoupling calibration methods, as described in sections III and IV.

### III. OPTIMIZATION OF SENSING COIL DESIGN

The sensing coil plays a key role in the performance of the inductive tri-axis force sensor. The inductance response of the

coils is highly dependent on coil geometry. In general, it is desirable to maximize the uncoupled inductance of the coils for a given spatial area which determines the measurement range (i.e. the maximum shift in sensor inductance due to the target movement). The sensitivity of the sensor is then a function of how the coils' baseline inductance changes during interaction with the conductive target. In this section, different coil patterns with different trace width, pitch, and shapes, are investigated to identify the optimal design for plantar load sensing.

#### A. Effect of Trace Width and Pitch on the Coil Inductance

Trace width and pitch determine the number of turns of a coil in a specific sensing area and thus affect the coil inductance. To investigate their effect, two widely researched coil topologies, i.e. the circular and the square coils illustrated in Fig. 4, are selected as representatives. Their outer diameters are kept same, i.e. 7 mm. The number of the coil turns is maximized according to the trace width and pitch. The coils inductances are simulated using an FE computational simulation (ANSYS Maxwell 3D module, full details of the model design and simulation are in Appendix A & B, coil geometries are specified in Appendix C). To simplify the modelling, single-layer coils are used but the results are consistent with multi-layer systems.

The simulated inductances of the circular coil and the square coil are plotted in Fig. 5. It can be seen that they



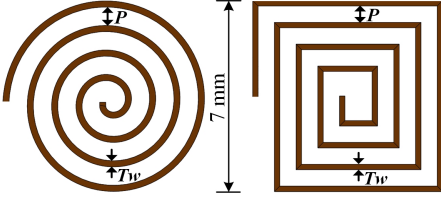
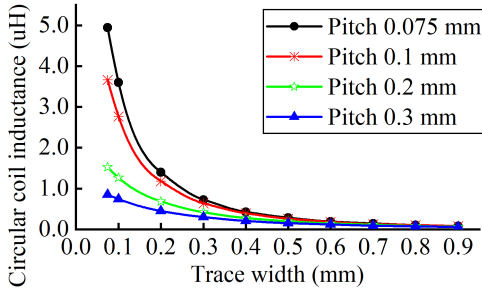
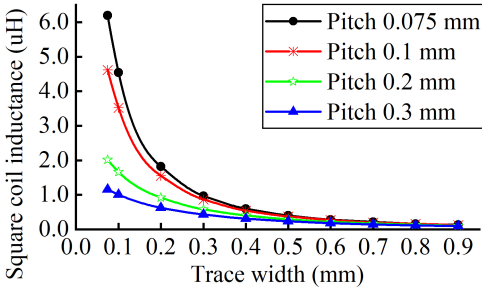


Fig. 4: Examples of coil topologies, with  $P$  being the pitch and  $Tw$  being the trace width.

demonstrate similar trends. As trace width increases, the coil inductance falls at a decreasing rate. With the reduction of pitch, the inductance increases. This can be explained by the fact that the number of coil turns and the total trace length (see Appendix C) reduce with an increase in pitch and trace width. Therefore, to maximize inductance, the coil should be designed to minimize pitch spacing and trace width (to permit more coil turns in a given area). This is typically bounded by current manufacturing constraints in which commercial printed circuit board (PCB) fabrication usually allows pitch and trace width no less than 0.1 mm.



(a) Inductance of circular coil with different trace width and pitch.



(b) Inductance of square coil with different trace width and pitch.

Fig. 5: The effect of the trace width and pitch to the inductance of the circular and square coils.

### B. Planar Coil Topologies of Tri-axis Inductive Sensor

To allow tessellation of the sensing nodes (e.g. in an insole-shaped sensing array for plantar load measurements), it is advantageous to employ a regular sensing geometry such as a rectangle or circle. The overall sensor size will then determine the spatial resolution which can be achieved. To address the requirements defined in Table I, the inductive sensors were designed with a square/circular sensing area of 15 mm  $\times$  15 mm or  $\varnothing$ 15 mm. As described in section II, the inductive sensors to be studied consist of three or four planar coils.

Three coil shape primitives were selected for investigation in each sensor configuration; circular, square and fan elements for the four-coil sensor design and circular, elliptical and fan coils for the three-coil sensor development. These primitives were identified through preliminary work as the most promising geometries to maximize coil turns and coil length within a particular sensing area. The schematics of the sensors to be studied are shown in Fig. 6. We set the trace width and pitch of the coils as 0.1 mm to meet typical manufacturing capabilities (see Section III.A). Design guidance for inductive coils specifies that the ratio of the coil's inner diameter ( $d_{IN}$ ) to outer diameter ( $d_{OUT}$ ) should be greater than 0.3 for a lower rate of energy loss [43]. This enables four circular coils, each with 12 turns ( $d_{OUT} = 7.0$  mm,  $d_{IN} = 2.2$  mm, see Fig. 6(a)&(b).i). For comparison, the other coil geometries were also designed with 12 turns. In addition, we also investigated the performance where the number of turns was maximized for each coil geometry. To enhance the coil inductance, all the coils shown in Fig. 6 were designed with double layers; the top layer in a clockwise rotation and the bottom layer in an anti-clockwise rotation, so that the magnetic fields positively add.

According to our previous research [31], the circular target passing through the center of all coils enabled the tri-axis inductive sensors to produce comparable sensitivity in all three axes. Therefore, an aluminum circular target is used in this research, sized to bisect the center of each coil under a zero displacement condition ( $\varnothing$ 11.3 mm for the four-coil inductive sensors and  $\varnothing$ 9.2 mm for the three-coil sensors, thickness 0.2 mm).

### C. Finite Element Modelling of the Tri-axis Sensors

An FE method was used to model and investigate the electromagnetic response of the different inductive sensor configurations shown in Fig. 6. Models were constructed in a computational package (ANSYS, see Appendix A) to obtain coil inductance for different axial displacements. The output inductances of all the four-coil sensors respond in a similar way to the example shown in Fig. 3(a) and the outputs of all the three-coil sensors are similar to that presented in Fig. 3(b). With the current spatial parameters, the sensors are generally sensitive to lateral displacements from -2 mm to 2 mm and vertical displacement below 2 mm, which is referred to as the operating volume for the inductive sensors in this paper. To compare the performance of the different sensors within this operating volume, a simplified methodology was used to compute the inductance along each axis, i.e.  $L_x$ ,  $L_y$ , and  $L_z$ . Equation (2) was used to decouple the outputs of the four-coil sensors and equation (3) was for the three-coil sensors. They are similar to the method used in [31], [42].

$$\text{Four-coil sensor} \begin{cases} L_x = -\Delta L_1 - \Delta L_2 + \Delta L_3 + \Delta L_4 \\ L_y = -\Delta L_1 + \Delta L_2 + \Delta L_3 - \Delta L_4 \\ L_z = (\Delta L_1 + \Delta L_2 + \Delta L_3 + \Delta L_4)/4 \end{cases} \quad (2)$$

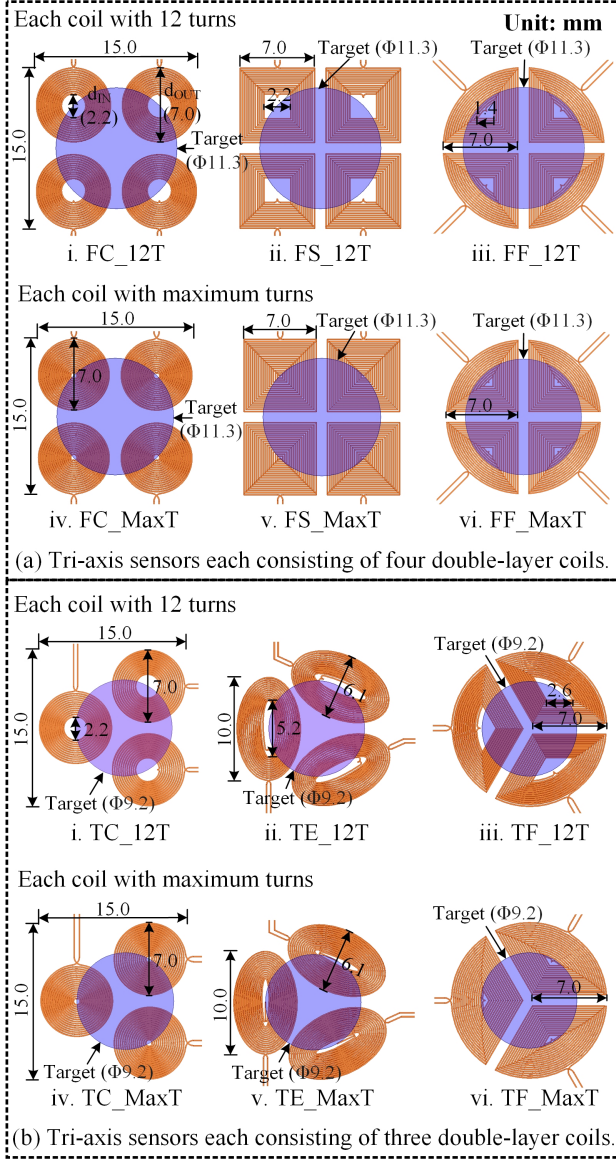


Fig. 6: Planar coil topologies of the tri-axis inductive sensors. (a) Each sensor consists of four double-layer coils, with a total sensing area of 15 mm × 15 mm; (b) each sensor consists of three double-layer coils, with a total sensing area of 15 mm × 15 mm. The abbreviations of ‘FC\_12T’, ‘FS\_12T’, ‘FF\_12T’, ‘TC\_12T’, ‘TE\_12T’, and ‘TF\_12T’ represent the four-circular-coil sensor, the four-squarer-coil sensor, the four-fan-coil sensor, the three-circular-coil sensor, the three-elliptical-coil sensor, and the three-fan-coil sensor with 12 turns, respectively; ‘FC\_MaxT’, ‘FS\_MaxT’, ‘FF\_MaxT’, ‘TC\_MaxT’, ‘TE\_MaxT’, and ‘TF\_MaxT’ represent the four-circular-coil sensor, the four-squarer-coil sensor, the four-fan-coil sensor, the three-circular-coil sensor, the three-elliptical-coil sensor, and the three-fan-coil sensor with the maximum turns, respectively.

$$\text{Three-coil sensor} \begin{cases} L_x = -\Delta L_1 + \Delta L_2 + \Delta L_3 \\ L_y = \Delta L_1 - \Delta L_2 + \Delta L_3 \\ L_z = (\Delta L_1 + \Delta L_2 + \Delta L_3)/3 \end{cases} \quad (3)$$

where  $L_x$ ,  $L_y$ ,  $L_z$  denote the inductive output along the x-, y-, and z-axis, respectively.  $\Delta L_i$  represents the difference between the coil output  $L_i$  and the coil inductance at free space  $L_{free\_i}$ , i.e.  $\Delta L_i = L_{free\_i} - L_i$  ( $i = 1, 2, 3, 4$ ).

The axial inductances of each sensor to the axial movements (vertical motion with  $dx$  and  $dy$  equal to zero and lateral motion with  $dz$  equal to 1 mm), are computed using (2) or (3). As shown in Fig. 7(a), the four-coil inductive sensors produced almost linear responses to the lateral movements but nonlinear outputs to the vertical motion. Conversely, the three-coil sensors showed linear outputs to the x-axis motion but nonlinear changes to both the y- and z-axis movements (see Fig. 7(b)). Additionally, the four-coil sensors all demonstrated larger inductance variation to the tri-axis motion of the target in comparison to the three-coil sensors. Among the three-coil sensors, TF\_MaxT exhibited the highest inductive changes to all the x-/y-/z-axis motion (1.1  $\mu\text{H}$ , 0.9  $\mu\text{H}$ , and 0.5  $\mu\text{H}$ , respectively), but lower than any one of the proposed four-coil sensors. Among the four-coil sensors, FS\_MaxT showed the largest variations in inductance (1.8  $\mu\text{H}$ ) to the lateral motion. For vertical movement of the target, FF\_MaxT and FF\_12T presented comparable inductance change (about 0.8  $\mu\text{H}$ ), higher than the other sensors.

The sensitivity of the tri-axis inductive sensors was calculated and summarized in Table II. In comparison with the three-coil sensors, the four-coil sensors generally demonstrated higher sensitivity to both the lateral and the vertical movements. Additionally, for a particular sensor configuration, maximizing the coil turns produced a higher sensitivity. Among these sensors, FS\_MaxT displays the highest lateral sensitivity but a lower vertical sensitivity. In contrast, FF\_MaxT shows the highest vertical sensitivity but a lower lateral sensitivity.

TABLE II: Sensitivity of the tri-axis inductive sensors at the specified motion range.

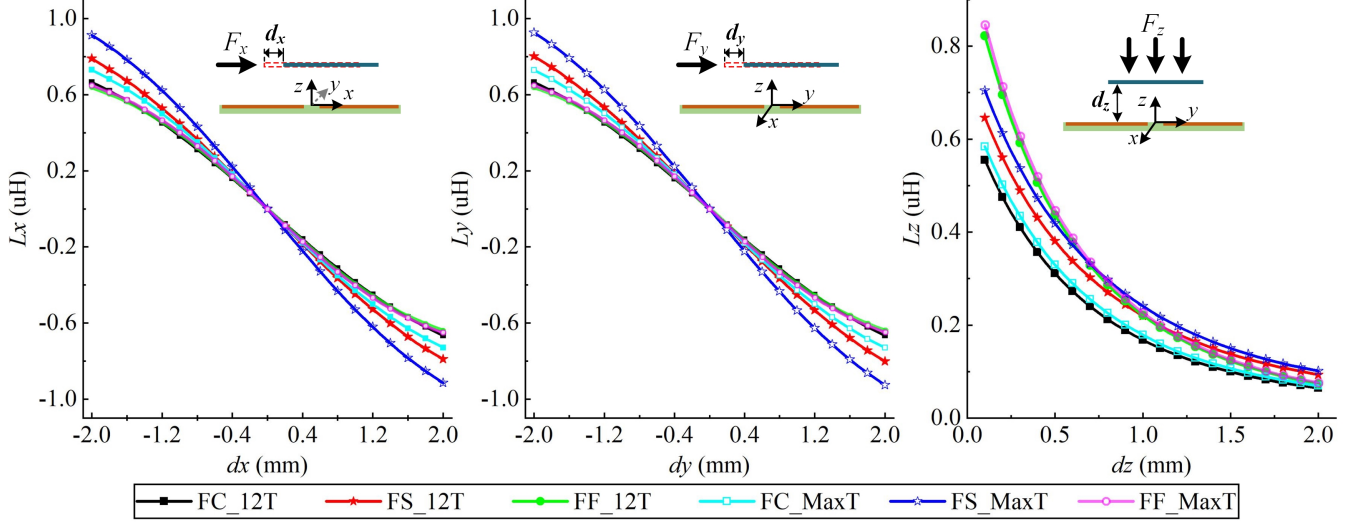
Inductive sensor	$S_x$ (nH/mm)	$S_y$ (nH/mm)	$S_z$ (nH/mm)
FC_12T	355.6	355.7	[86.2, 566.4]
FC_MaxT	392.9	393.0	[112.4, 736.2]
FS_12T	419.1	423.8	[72.7, 592.0]
FS_MaxT	<b>489.1</b>	<b>494.6</b>	[74.1, 644.1]
FF_12T	353.1	353.1	[179.6, 1169.9]
FF_MaxT	358.3	358.1	<b>[187.1, 1210.0]</b>
TC_12T	214.5	[71.7, 297.3]	[85.0, 555.4]
TC_MaxT	236.1	[81.5, 323.6]	[108.1, 716.5]
TE_12T	251.9	[56.9, 365.5]	[44.5, 382.6]
TE_MaxT	289.8	[69.5, 419.7]	[40.8, 415.9]
TF_12T	265.3	[96.3, 362.9]	[56.6, 502.1]
TF_MaxT	294.1	[115.0, 396.9]	[71.2, 579.4]

The maximum and the minimum values of the inductance, the quality factor ( $Q$ ), and the equivalent parallel resistance ( $R_p$ ) of each coil pattern are presented in Table III.  $Q$  is a measure of a coil’s efficiency and  $R_p$  determines the drive current required for a measurable oscillating amplitude, which are defined in (4).

$$R_p = \frac{(2\pi f L)^2}{R_s} \quad (4)$$

$$Q = \frac{2\pi f L}{R_s} = \frac{R_p}{2\pi f L}$$

(a) The four-coil sensors' responses.



(b) The three-coil sensors' responses.

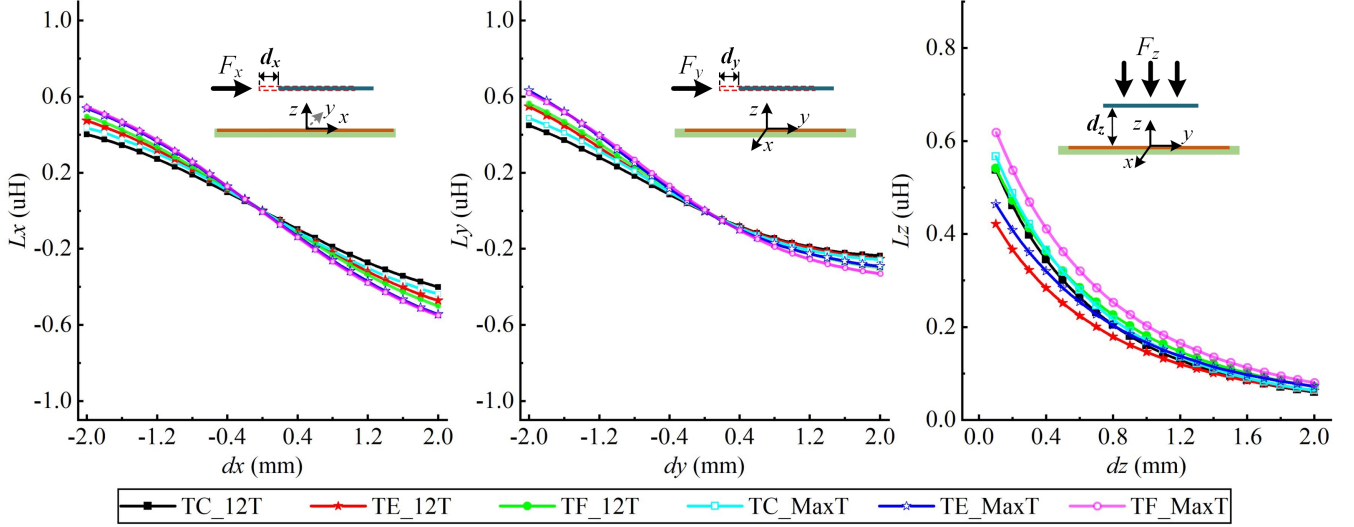


Fig. 7: The inductive responses of the proposed sensors to the tri-axis movement of the target.

where  $R_s$  and  $L$  represent the series resistance and the inductance of coil, respectively. The parameter  $f$  denotes the operating frequency.

Each sensing coil produces the largest  $L$ ,  $R_p$ , and  $Q$  at the operating frequency when at free space (i.e. without target); in the operating volume, the minimum values of  $L$ ,  $R_p$ , and  $Q$  are generated as the coil has the maximum overlapping with the target. Table III shows that for any configuration, using maximal coil turns produces higher inductance but lower parallel resistance  $R_p$  and quality factor  $Q$  than a 12-turn equivalent. This occurs because the coil's innermost turns contribute less to the overall inductance than the outer turns but still increase the equivalent series resistance  $R_s$ , thus decreasing  $R_p$  and  $Q$ . Among these sensors, FF\_12T and FF\_MaxT demonstrated the lowest  $R_p$  and  $Q$ , indicating a high-energy dissipation; the four-square-coil sensors (FS\_12T and FS\_MaxT) and the three-fan-coil sensors (TF\_12T and

TF\_MaxT) presented comparable values of  $R_p$  and  $Q$ , generally higher than the others, showing their great capability of energy storage.

Overall, considering factors of baseline inductance, target sensitivity, and  $Q$  factor, the four-coil sensors consistently outperform the three-coil sensors for tri-axis motion. From the proposed twelve tri-axis sensor designs, FS\_MaxT is best suited to measure plantar load distribution due to its high sensitivity, low energy dissipation, and low current required to maintain oscillation.

#### IV. SENSOR FABRICATION AND EVALUATION

##### A. Sensor Prototyping

An inductive tri-axis force sensor was developed from the ideal configuration (FS\_MaxT) identified in section III. The design consists of four-square double-layer coils. The coils were fabricated on a 25  $\mu\text{m}$  thick Kapton polyimide film using



TABLE III: The inductance, the AC parallel resistance  $R_p$  and the quality factor  $Q$  of each sensor at a typical operating frequency of 6.2 MHz.

Sensor	Maximum			Minimum		
	L ( $\mu$ H)	$R_p$ (k $\Omega$ )	Q	L ( $\mu$ H)	$R_p$ (k $\Omega$ )	Q
FC_12T	2.56	4.06	50.5	0.66	0.16	8.0
FC_MaxT	2.78	3.87	44.3	0.70	0.17	7.8
FS_12T	3.13	5.00	50.6	0.91	0.26	9.0
FS_MaxT	3.51	5.05	45.8	0.99	0.27	8.8
FF_12T	2.14	2.66	39.6	0.55	0.12	7.0
FF_MaxT	2.18	2.64	38.6	0.56	0.12	7.0
TC_12T	2.57	3.93	48.7	0.57	0.13	7.0
TC_MaxT	2.79	3.84	43.9	0.63	0.14	7.1
TE_12T	3.26	5.15	50.4	0.82	0.20	7.8
TE_MaxT	3.69	5.54	47.9	0.91	0.22	7.8
TF_12T	3.26	4.93	48.1	0.94	0.26	8.7
TF_MaxT	3.52	4.94	44.6	1.00	0.27	8.6

a standard flexible PCB manufacturing process, located in an area of 15.0 mm  $\times$  15.0 mm and with a total thickness of 0.23 mm, as shown in Fig. 8. A circular aluminum disc ( $\phi$ 11.3 mm, thickness 0.2 mm) was laser-cut as the sensing target. A 2-mm thick silicon sheet (Smooth-Sil™ 950, Smooth-On Inc., USA) was selected as the elastic medium between the coils with the target due to its mechanical properties providing appropriate response under loading [44]. For the silicon fabrication, first, two parts of the silicon liquids (10A:1B weight) were mixed and deaerated using a non-vacuum mixer (ARE-310, Thinky Inc., Japan). Then, the mixture was poured into an acrylic mold with a 2-mm thickness. Once the silicon was spread uniformly, it was left at the room temperature to cure. A circular elastomer ( $\phi$ 11.3 mm) was then cut from the sheet using a laser-cutter (VLS3.50, Universal Laser Systems).

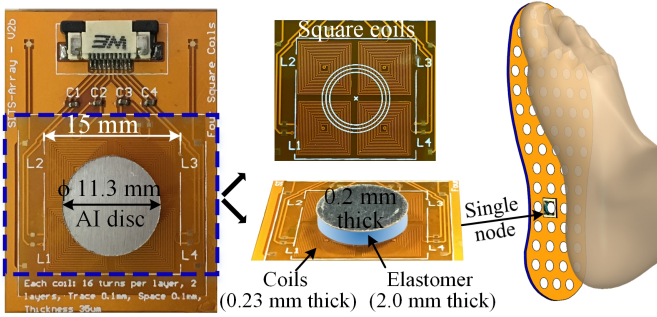


Fig. 8: An integrated tri-axis inductive sensor prototype.

The sensor was finally assembled using cyanoacrylate glue to affix conjoined layers and alignment masks to ensure precise alignment of the target and elastomer relative to the coils. Fig. 8 shows an assembled prototype of the resultant tri-axis inductive force sensor.

### B. Electronic Interface

To obtain the external load applied to the sensor, the coils' inductances need to be measured and post-processed. As described in section II, a four-channel inductance to digital

converter chip (LDC1614, Texas Instruments, USA) was used to drive the L-C circuit and measure its oscillation frequency (see the schematics shown in Fig. 9). This chip is capable of operating at an oscillation frequency of 1 kHz to 10 MHz. In the operating volume of the tri-axis sensor prototype, the minimum inductance of each square coil is 0.99  $\mu$ H. Thus, to keep the coil oscillation below 10 MHz, an external capacitor with a minimum capacitance of 256 pF is required. A 330 pF C0G/NP0 capacitor was selected for this purpose (from typical capacitance values), resulting in an L-C circuit which resonates at a frequency ranging from 4.7 MHz (maximum inductance 3.51  $\mu$ H, without loading) to 8.8 MHz (minimum inductance, fully loaded) during the multi-axis motion. A real-time embedded evaluation board (NI MyRIO-1900 [45]) was used to communicate with the LDC1614 through an I2C bus.

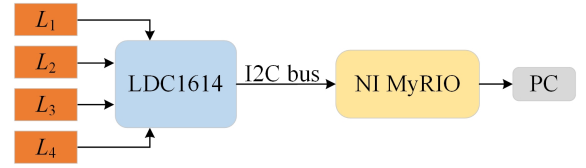


Fig. 9: The electrical interface for the developed tri-axis inductive sensor.

### C. Experimental Set-up

To characterize and evaluate the sensor prototype, an experimental setup was developed to apply multi-axis loading to the sensor. This consists of three linear translation stages (MTS50-Z8, Thorlabs Inc., UK) in the configuration shown in Fig. 10. The translation stages are controlled by single-channel DC servo motor controllers (KDC101, Thorlabs Inc., UK), providing a travel range of 50 mm along each motor axis. This system can move at the velocity up to 2.4 mm/s. The minimum repeatable incremental movement is 0.8  $\mu$ m and the repeatability is 1.6  $\mu$ m for bidirectional motion. A commercially available 6-axis force/torque sensor (Nano25, ATI Industrial Automation Inc., Apex, NC, USA) was used as a load reference for the calibration and evaluation of the sensor prototype. It has a force measurement range of  $\pm 250$  N in the x/y-axis and  $\pm 1000$  N in the z-axis, with a resolution down to 21 mN. The full system, illustrated in Fig. 10, places the load cell and an indenter on the Z stage while the sensor prototype is fixed onto the XY stage. The system applies load to the sensor prototype through controlled displacement along the three axes as required. Motion in each axis is synchronized to allow off-axis loading of the sensor (e.g. through simultaneous movement in the X and Z axes). The resultant force obtained from the load cell is then used to calibrate the inductive sensor. A custom program was developed for measurement and control of the calibration system and logging the resultant data for post-processing (LabVIEW, National Instruments).

### D. Evaluation of the Sensor's Inductive Response

An experimental study was undertaken to examine the sensor's inductance response within the operating volume and

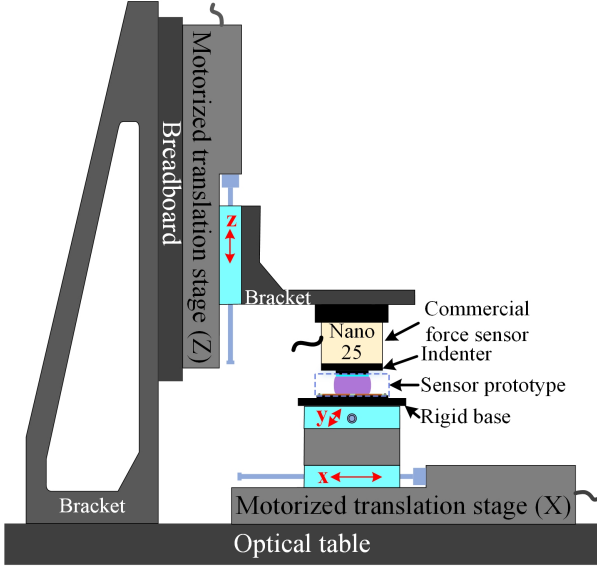


Fig. 10: Configuration of the multi-axis sensor calibration system.

validate the computational FE models (i.e. neglecting force load information). The target was fixed on the indenter and the coil system placed onto the rigid base. Elements were center-aligned and initially spaced 2 mm apart. The Z-axis translation stage was controlled to move the target from the initial position to 0.1 mm away from the sensing coils at an increment of 0.1 mm ( $dx = dy = 0$  mm). The inductance of the sensing coils was measured after each increment was complete. This procedure was repeated five times. Similarly, the coils' responses to the lateral movement of the target was investigated in the range of -2 mm to 2 mm with an increment of 0.1 mm ( $dz = 0$  mm).

The inductance along each motion axis was computed and plotted in Fig. 11, together with the corresponding simulation results for comparison. It can be seen that the model results are in close agreement with the experimental data within these movement parameters. They demonstrate a maximum difference of 2.71% FS and a root mean square error (RMSE) of 8.0 nH to motion in the z-axis. In the x-axis and y-axis movements, the differences did not exceed 2.1% FS and 1.6% FS, and the RMSE was 5.6 nH and 4.8 nH, respectively.

#### E. Sensor Calibration for Force Measurement

A calibration process was performed to characterize the sensor's response to applied external loads. The importance of rigorous calibration for this sensor is highlighted by the strong inter-axis coupling evident in the responses shown in Fig. 7(a) and Fig. 11. For example, for  $dz = 1$ ,  $L_x$  varied 1.83  $\mu$ H between  $dx = -2:2$  mm but for  $dz = 2$  mm it only changed 0.6  $\mu$ H. This is typical of the response in each axis.

The calibration process used the multi-axis calibration system shown in Fig. 10. A 3D scanning process was conducted to fully investigate the relationship between coil inductance and applied force throughout the sensor operating volume. The volume was swept by stepping through each axis in 0.1 mm increments, led by increasing indentation from  $dz = 2$  mm to

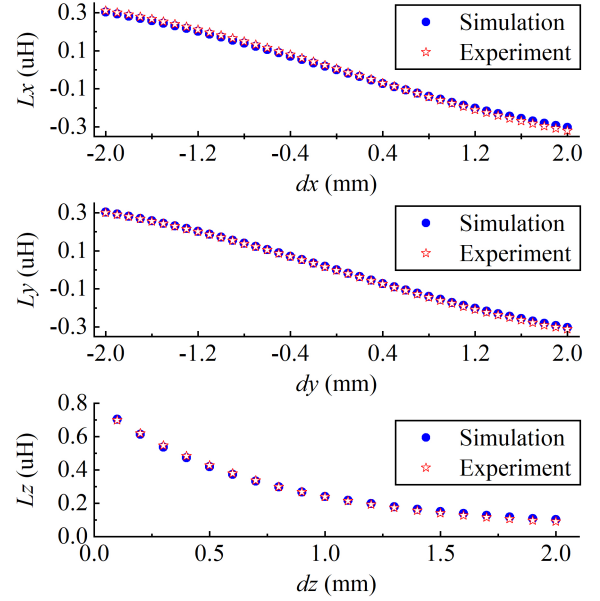


Fig. 11: Validation of the sensor's responses to the displacement variations along each axis.

1.4 mm, with  $dx$  and  $dy$  swept between -1:1 mm for each  $dz$  setting. The coil inductances and resultant load were then recorded at each increment in a quasi-static fashion. Fig. 12 shows an example of the inductance response for all four coils as varying axial loading is applied to the sensor prototype. The coupled trend of the coils is clear, with slight inductance variations between the coils due to imperfect alignment of the inductive target (e.g. it is marginally off-centre at zero load).

Due to the complex relationship between the applied multi-axis force and measured inductance outputs, a two-layer feed-forward neural network was selected to characterise the sensor [46]. The network is shown in Fig. 13(a), which comprises of 15 neurons in the hidden layer, the Tanh function as the activation function and the Levenberg-Marquardt backpropagation algorithm used as the training method. These features were selected based on prior research [47], [48] and preliminary testing for the identification of an appropriate structure. A total of 143172 data samples were obtained during the loading and unloading calibration process, of these 70% of the samples were used for training, 15% for validation, and the remaining 15% for testing.

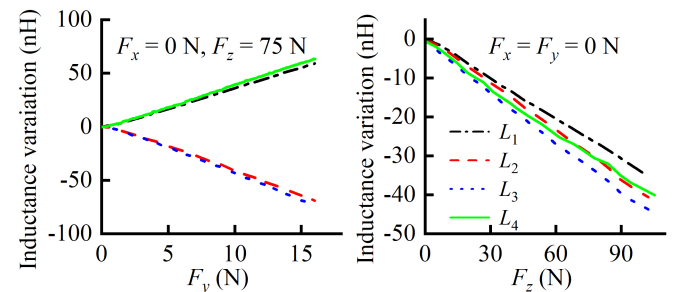


Fig. 12: An example of the variation in coil inductances under varying load.



The estimated force output using the calibration neural network is presented in Fig. 13(b) (here  $F_x$  is omitted because symmetry results in a similar distribution to  $F_y$ ). As shown in Fig. 13(b), the shear load  $F_y$  increased with increasing  $dy$  and the absolute value of  $F_y$  was maximum at the positions with  $dy$  equal to -1 mm or 1 mm. The normal load increased as the target approached the sensing coils. In relation to the reference load cell, the readings of the sensor prototype present a RMSE of 1.05 N ( $F_x$ ), 1.05 N ( $F_y$ ), and 1.73 N ( $F_z$ ). The larger deviation in  $F_z$  may be co-related to temporal drift characteristics of the reference load cell (without loading this demonstrated a drift of  $\sim 0.3$  N and 0.1 N over 2 hours in normal and shear loading axes, respectively).

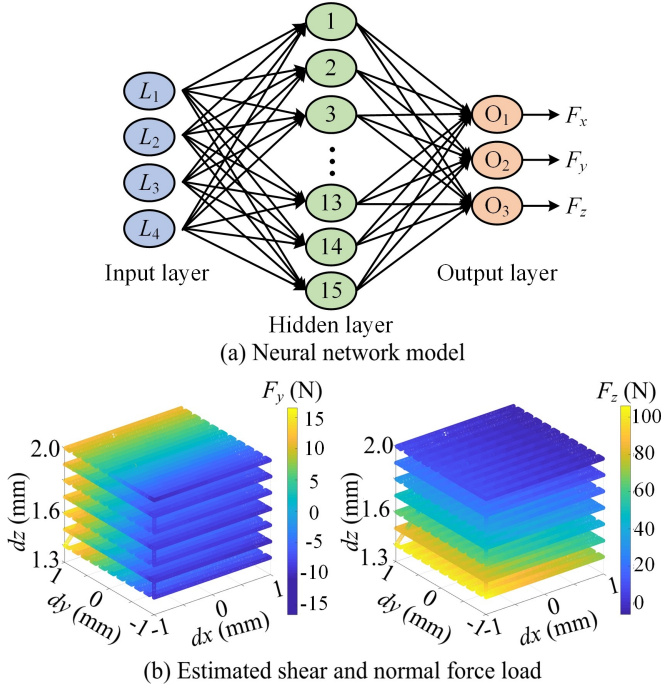


Fig. 13: (a) Structure of the two-layer neural network model used to calibrate sensor output, (b) estimated normal and shear load using the Neural Network model in the defined movement volume.

### F. Sensor Evaluation for Force Measurement

To assess the capability of the sensor prototype for measuring external load, tests were carried out to characterise the sensor, comprising temporal drift, hysteresis, and dynamic response.

1) *Temporal drift of the sensor prototype*: To evaluate the sensor's temporal stability, a range of multi-axis loads (between 10%-60%FS for each axis) were applied to the sensor prototype for 180 min while the sensor output inductances were measured and converted into force values using the calibration neural network. In these tests, the sensor prototype showed variations typically no more than 3 mN for  $F_x$  and  $F_y$  (0.02%FS) and 6 mN for  $F_z$  (0.01%FS), indicating that the sensor prototype has low temporal drift. Fig. 14(a) presented the results obtained in one of these tests as a representative case.

2) *Hysteresis of the sensor prototype*: The sensor response is dependent on the compressible elastomer layer. Elastomeric materials are known to experience elastic hysteresis, typically due to internal material friction. We therefore evaluated the sensor hysteresis, achieved by applying a low frequency (0.05 Hz) cyclic load to the sensor prototype. As shown in Fig. 14(b), the sensor prototype showed a maximum hysteresis of 4.7%FS for the cyclic shear loading with an amplitude of 15.9 N and 5.8%FS under normal loading (amplitude 105 N), slightly higher than the hysteresis error of the soft sensor presented in [49] (4.3% FS for normal loading) and [50] (3.2% for normal loading and 4.0% for shear loading). These hysteresis properties can be altered and optimised through modification of the compressible layer, for example using different elastomeric materials. This is a topic of ongoing research within our group.

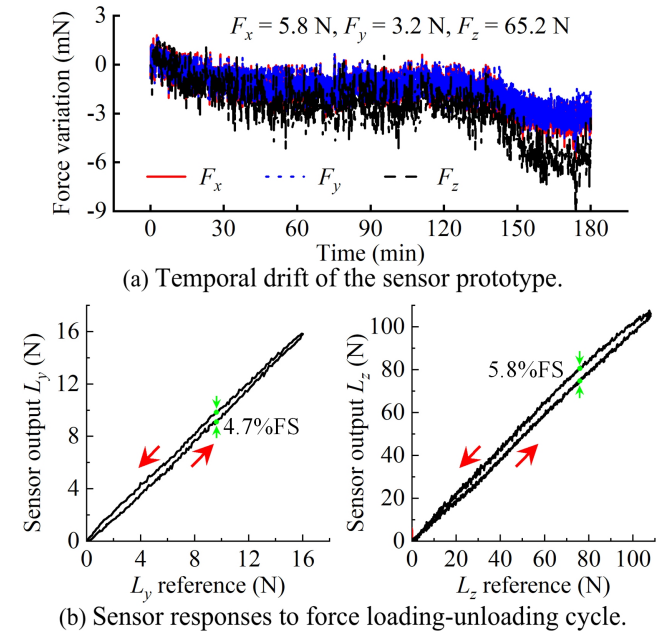


Fig. 14: (a) Temporal (drift) response of the sensor prototype under multi-axis loading for 180 minutes, (b) Hysteresis response of the sensor to shear and normal loading-unloading cycles.

3) *Sensor dynamic response*: The dynamic response of the sensor prototype is important for its practical application to monitor plantar load across the foot during daily activities. The literature shows that people walk with different stride frequencies but usually in the range of 1.4-2.5 Hz [51]. When running, stride frequency can be up to 4.8 Hz [52]. Therefore, tests were conducted to investigate the dynamic response of the sensor under different load regimes. The multi-axis load response was explored using the multi-axis calibration system (Fig. 10). The three axes were swept simultaneously at a velocity of 0.25 mm/s (about 0.17 Hz) to produce a varying tri-axis load to the sensor prototype across the operating load range. The sensor output inductances were measured at 100 Hz and converted into corresponding force values. Fig. 15 presents these data, together with the applied load determined by the reference load cell. It is evident that the calibrated sensor

exhibits close agreement to the reference, showing an RMSE of 0.26 N for  $F_x$  measurements and 1.37 N for  $F_z$ . Some significant variations were observed at points of peak force, likely due to increased hysteresis in the elastomeric layer of the sensor in comparison to the reference load cell which uses silicon strain gauges.

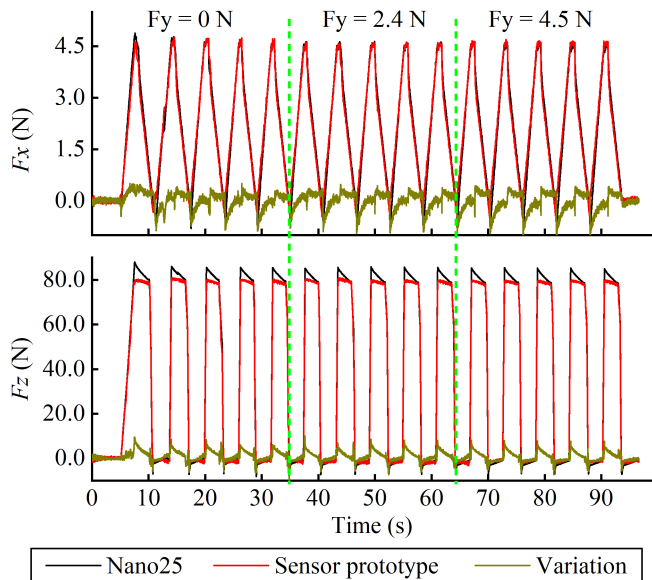


Fig. 15: Responses of the sensor prototype and the commercial force sensor (Nano25) to the varied tri-axis load.

We further evaluated dynamic performance at increased frequencies using a dynamic loading instrument (Instron ElectroPuls™ E10000 with load cell 105393, capable of performing motion up to 100 Hz). This system is limited to single-axis motion, so a cyclic normal load was applied to the sensor prototype. The system was configured under position control mode to successively apply triangular waveforms across frequencies of 1 Hz, 3 Hz, 6Hz and 10 Hz. The applied load and the sensor outputs were measured simultaneously at a sample rate of 250 Hz. As shown in Fig. 16, the sensor prototype closely followed the load profile across the tested frequencies of 1 Hz, 3 Hz, 6Hz, and 10 Hz, demonstrating an RMSE of 1.55 N, 1.69 N, 1.81 N, and 2.76 N, respectively. Phase lag is negligible at these operating frequencies. In each cycle, a plateau is evident at the position where  $F_z = 0$  N where the indenter briefly loses contact with the sensor. The sensor's response to multi-axis loading at these higher frequencies will be explored using specialized equipment in future work.

## V. DISCUSSION

This paper demonstrates how multi-axis inductive sensing technology can be readily tailored toward a specific application, in this instance to address the clinical need of measuring foot loading to assess diabetic foot ulceration. This involves firstly mapping the clinical needs to a set of technical specifications, and secondly understanding how (and if) these can be achieved given the sensor's design parameters and constraints. 3D FE modelling has formed the core of the design

and optimization process to ensure the sensor is appropriate for plantar load measurement. As presented in section III, the developed 3D model provides a tool to understand the influence of the design parameters including symmetric and non-symmetric configuration of multiple coils, their individual design, and electrical energization of the coil system. Validation of the model showed that the simulated results from these 3D models were consistent with the response from a representative experimental configuration (see Fig. 11). Using this model-based optimization approach has facilitated the navigation of complex and coupled mechanical, electrical and electromagnetic factors which comprise the sensor's design-space. The arrangement of four-square sensing coils with maximal turns was found to be the most suitable design for the requirements of plantar load measurement which has the particular need for sensitivity in both normal and shear loading. The 3D model also helped define the sensor's effective operating volume ( $-2 \text{ mm} < dx, dy < 2 \text{ mm}$ ,  $dz < 2 \text{ mm}$ ) based on the sensitivity constraints and sensor size requirements for effective measurement of plantar load.

The tri-axis sensor produces a non-linear response between applied load and the direct measurements of coil inductance, combined with strong inter-axis coupling. Calibration therefore requires careful consideration of these characteristics. Our previous work has employed genetic algorithms [31] but here a two-layer feed-forward neural network model was found to provide a superior response, in particular the avoidance of overfitting characteristics. Experimental evaluation (see Fig. 13 and Fig. 15) demonstrate that the neural network approach successfully decoupled the sensor outputs to provide an accurate mapping to the applied load. The same trained neural network can then be applied to calibrate each sensing node in an array because they act as independent elements (as shown in Fig. 8). This approach provides a computationally efficient solution to calibration of the sensing array; the training process is computationally expensive but needs only be conducted once and prior to use, subsequently it is feasible to reconstruct output loads online using the trained neural network on an embedded system.

The optimized and calibrated sensor prototype successfully meets the essential requirements for plantar load measurement shown in Table I. As demonstrated in Fig. 13(b), the sensor is capable of measuring a normal load of 0-105 N (equivalent to 0-1047 kPa pressure, the perpendicular component of force per unit area over which the force is distributed) and shear load from -16 N to 16 N (equivalent to -160-160 kPa shear stress, the horizontal component of force per cross-sectional area). This outperforms the measurement range of similar tri-axis force sensors reported for plantar load detection in the literature [26] (131 kPa in each axis), [27] (250 kPa for pressure and 31 kPa for shear axes), [28] (11.8 kPa, 11.3 kPa, and 15.7 kPa in the x-, y-, and z-axis, respectively), and [31] (84.5 kPa for pressure and 9.1 kPa for shear stress). The size of the sensor is also critical and the reported prototype has overall dimensions of  $15 \text{ mm} \times 15 \text{ mm} \times 2.5 \text{ mm}$ , comparing favourably to the sensors reported above. In addition, the sensor prototype presented appropriate characteristics for load measurement with low drift (high temporal stability, see Fig.

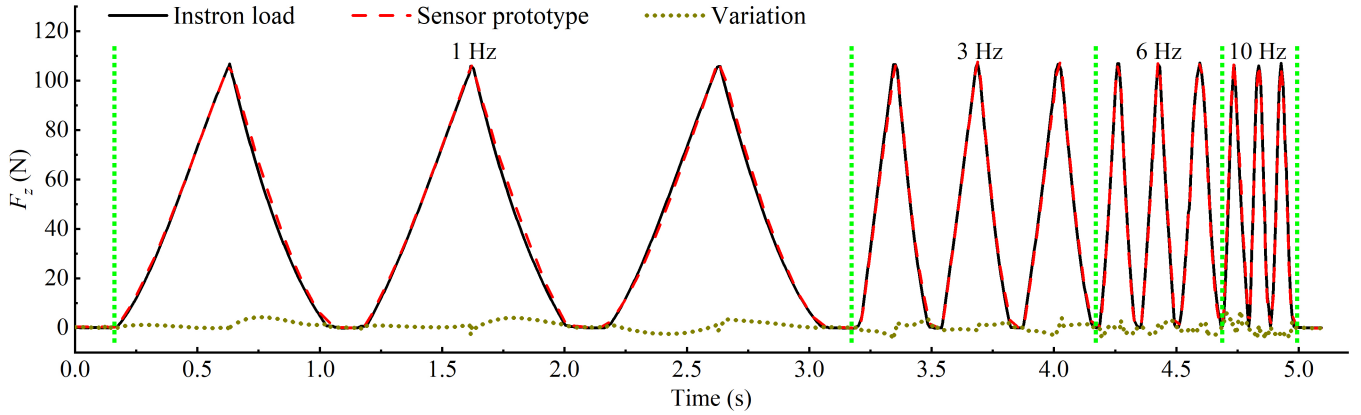


Fig. 16: Response of the sensor prototype to cyclic normal force load with a frequency of 1 Hz, 3 Hz, 6 Hz, and 10 Hz.

14(a)) and a good dynamic response in the target frequency range (see Fig. 15 and Fig. 16). These traits indicate the strong potential for this sensing technique to be used for plantar load measurement of the foot.

The main limitations of the sensor presented here relate to performance and robustness. At 2.5mm thick, the sensor prototype presented here operates at the outer limit of the operating volume defined in section III.C ( $-2 \text{ mm} \leq dx, dy \leq 2 \text{ mm}$ ,  $0 < dz \leq 2 \text{ mm}$ ), limiting sensitivity. The overall thickness is dominated by the 2 mm thick elastomer layer. In this phase of research, a manual molding technique was used to fabricate the elastomer layer, placing a constraint on creating thinner layers. However, alternative semi-automated processes (e.g. using 3D printing and vacuum casting) can readily achieve consistent  $<2\text{mm}$  elastomer layers and provide a future means to reduce sensor thickness. This would bring improved sensor sensitivity (see Fig. 7) and reduce the sensor profile to be comparable to that of commercial load measurement insoles. For context, Tekscan's F-Scan system uses thin-film approaching 0.15 mm thickness but is not intended for sustained long-term use, more comparable is Novel.de's Pedar system at 1.9 mm thick. Using a similar configuration for this sensor technology would enable integration within an insole to ensure robustness for longevity while maintaining comfort. In conjunction, electrical robustness and wiring complexity are key challenges with this sensing technology, particularly when scaling up towards the target application of an array of sensors embedded within an insole. In this configuration, each sensing node will be spaced a few millimeters apart and each sensor's coils will be activated and measured sequentially to minimize mutual coupling and interference. To mitigate the effects of wiring complexity, we are exploring the combination of sensing coils and associated measurement electronics within an integrated PCB [53].

The focus of this current work has been to develop an appropriate 'sensing unit' that can form the basis of an in-shoe sensing array. The next stage of our research will be to develop and evaluate an integrated in-shoe sensing array. This will encompass further application specific evaluation including the sensor's dynamic response to multi-axis loading within a composite insole structure, aging effects, sensitivity

to the operating environment (e.g. temperature and humidity associated within a shoe), the arrangement of elements within the sensing array to ensure appropriate coverage of the plantar surface and reconstruction of the distributed load applied to the insole using the response from the sensing array, and inter-sensor variability (e.g. as a result of fabrication inconsistencies) and their correction using biasing techniques [54], [55]. It is pertinent to address and evaluate these aspects as an integrated system, since they are tightly coupled. For example, encapsulation of sensing elements within other materials for environmental protection will affect the sensor's dynamic response. Thus, this work represents a promising first step in the journey towards using inductive sensing technology for multi-axis plantar load measurement and the assessment of diabetic foot disorders.

## VI. CONCLUSION

This paper reports the design and the performance of a soft tri-axis inductive force sensor, the first of its kind suitable for simultaneous measurement of plantar normal and shear load. A 3D FE model was developed and validated as a valuable tool with which to optimise the sensor design parameters. A coil configuration using four-square coils with maximal turns in the specified sensing area outperformed other alternatives, showing both a high sensitivity to tri-axis loading and a high sensing quality-factor 'Q'. A neural network model was used to successfully calibrate the sensor and account for strong inter-axis coupling between the directly measured inductance parameters. Validation showed a close mapping between measured and applied loading. The final sensor prototype was fabricated with a dimension of  $15 \text{ mm} \times 15 \text{ mm} \times 2.5 \text{ mm}$  and could measure normal load up to 105 N (equivalent to 1047 kPa pressure) and shear load in the range of -16 N to 16 N (equivalent to -160-160 kPa shear stress) with a high temporal stability and a good dynamic response at target frequencies. This meets the expected load and spatial resolution requirements for measurement of multi-axis plantar loading. Overall, the reported tri-axis force sensor shows promise for use as an in-shoe load sensing node to assess people at risk of diabetic foot ulceration.

## APPENDIX

## A. Coil model design and performance simulation

In ANSYS Maxwell 3D module, basic structures can be created using geometric primitives together with geometry operations. Designing coils with a complex structure is a challenge with the built-in geometric tools, but a model can be designed externally and imported into the Maxwell package. We design the coil model and carry out the simulations following the steps below.

- 1) Develop a 3D model of the sensing coils in a CAD package and export in STEP format.
- 2) Import the 3D coil object into ANSYS Maxwell 3D environment.
- 3) Check the imported model. If the 3D coil model is an assembly drawing, each part will be imported as an individual geometric object in ANSYS Maxwell 3D. The relevant objects need to be united as a complete model. See Fig A1.
- 4) Create a boundary box surrounding the coils for simulation.
- 5) Bring the coil terminals out to touch the boundary edges.
- 6) Set the solution type, assign materials, excitations, mesh, and parameters for the coil objects, and add solution setup for analysis.
- 7) Set Optimetrics if necessary.
- 8) Perform a validation check before analysing the model.
- 9) Evaluate the simulated results.

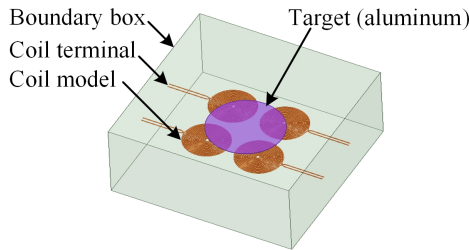


Fig. A1: 3D simulation model of a sensing coil design in ANSYS Maxwell environment

## B. Coil design for prototype fabrication

According to the following steps, the electronic circuit design was performed for coil prototype fabrication.

- 1) Develop 3D coil model in SolidWorks.
- 2) Save the coil design as a DXF/DWG file (all splines need to be exported as polylines). Before saving the DXF/DWG file, either the inner edges or the outer edges of the coil traces need to be deleted to get a single spiral trace line.
- 3) Import the coil files into PCB design software (e.g. Altium Designer).
- 4) Add soldering pads, vias, and extra traces for connection using the design tools in PCB software. If there exist some other components in the circuit design, all the electrical connections have to be finished before fabrication.

## C. Coil parameters

The parameters of the circular and square coils investigated in section III.A, including the pitch ( $P$ ), the trace width ( $T_w$ ), and the resultant trace length ( $L$ ), are listed in Table A. 1 (unit: mm).

TABLE A1: Parameters of the circular and square coils studied in section III.A.

$L \backslash P$	$T_w$	Circular coils				Square coil			
		0.075	0.1	0.2	0.3	0.075	0.1	0.2	0.3
0.075		252	217	138	102	331	285	186	139
0.1		215	188	126	94	284	250	170	130
0.2		133	122	92	74	179	166	127	103
0.3		95	89	71	59	130	124	101	86
0.4		72	69	58	49	102	98	84	73
0.5		58	56	48	42	84	81	71	64
0.6		48	47	41	36	71	69	62	56
0.7		41	38	35	31	62	58	54	50
0.8		35	34	30	29	54	53	49	44
0.9		30	30	28	25	48	48	43	41

## ACKNOWLEDGMENT

The research is supported by the National Institute for Health Research (NIHR) infrastructure at Leeds. The views expressed are those of the author(s) and not necessarily those of the NHS, the NIHR or the Department of Health and Social Care.

The authors would like to thank the NIHR MedTech and In Vitro diagnostics Co-operatives (MICs).

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