

1 **Effects of prophylactic knee bracing on knee joint kinetics and kinematics during single**  
2 **and double limb post-catch deceleration strategies in university netballers.**

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18

19 **Abstract**

20 *PURPOSE:* The aim of the current investigation was to investigate the effects of a  
21 prophylactic knee brace on knee joint kinetics and kinematics during single and double limb  
22 deceleration tasks. *METHODS:* Twenty female university first team level netballers  
23 performed single and double limb deceleration tasks under two conditions (prophylactic knee  
24 brace/ no-brace). Biomechanical data was captured using an eight-camera 3D motion capture  
25 system and a force platform. Participants also subjectively rated the comfort/ stability  
26 properties of the brace and their knee joint proprioception was examined with and without the  
27 knee brace using a weight bearing joint position sense test. *RESULTS:* The results showed  
28 that during both single and double limb deceleration tasks neither peak anterior cruciate  
29 ligament (brace: single=1.30 / double=1.30 bodyweight (BW) & no-brace: single=1.19 /  
30 double=1.29 BW)  $P=0.51$ , patellofemoral (brace: single=4.21/ double = 4.93 BW & no-  
31 brace: single=3.99 / double=4.63 BW)  $P=0.20$  or patellar tendon (brace: single = 6.17/  
32 double=6.49 BW & no-brace: single=6.07 / double=6.14 BW)  $P=0.49$  kinetics were  
33 significantly affected as a function of wearing the knee brace. The findings also showed that  
34 the knee brace helped to increase participants perceived knee stability ( $P<0.001$ ) but there  
35 were no statistical improvements in weight bearing knee proprioception (brace=3.59 & no-  
36 brace=2.94°)  $P=0.44$ . *CONCLUSIONS:* The current investigation indicates that the utilization  
37 of prophylactic knee bracing akin to the device used in the current study does not appear to  
38 reduce the biomechanical parameters linked to the aetiology of knee injuries, during netball  
39 specific deceleration movements.

40

## 41 **Introduction**

42 Netball is representative of a team based global sporting discipline, with participation in over  
43 70 countries (1). Like most court sports netball is a physical challenging activity

44 characterized by a series of high intensity dynamic movements; although unlike most court  
45 based disciplines there are additional physical considerations imposed by the specific rules of  
46 the sport (2). Particularly as players must stop completely upon receiving the ball which  
47 places considerable emphasis on rapid deceleration manoeuvres (2).

48

49 Indeed, netball has been shown to be associated with a high rate of non-contact injuries.  
50 During tournament play 238 injuries were observed per 1000 playing hours (3) and an injury  
51 rate of 66.7–71.4 per 1000 participants has been noted from a retrospective analysis of three  
52 competitive seasons (4). These analyses have shown that the majority of injuries occur in the  
53 lower extremities; with the knee being the most commonly injured musculoskeletal structure  
54 in netball players, accounting for 24 % of total injuries (3, 5). Importantly, a systematic  
55 review of knee pathologies identified rapid deceleration manoeuvres as one of the three  
56 movements that may lead to knee injury (6).

57

58 Single and double limb landing manoeuvres generate large impact forces that are primarily  
59 attenuated in the lower extremities joints, with particular stress at the knee joint (7). The knee  
60 joint structures considered at greatest risk from chronic and acute pathologies during rapid  
61 deceleration tasks are the anterior cruciate ligament (ACL), patellofemoral joint and patellar  
62 tendon (8, 9, 10). Over 250,000 ACL injuries occur annually, causing long term absence from  
63 training (11), and allocated healthcare costs of over \$3.4 billion (12). Biomechanically, the  
64 predominant risk factors for non-contact ACL pathologies are a reduced knee flexion angle at  
65 initial contact, large knee valgus angle, large knee internal rotation angle and excessive forces  
66 experienced by the ligament itself (11, 13, 14). In addition, patellofemoral pain accounts for a  
67 quarter of all injuries treated in sports medicine clinics, and is strongly linked to the aetiology

68 of osteoarthritis at this joint (15). Kinetic and kinematic risk factors identified as predictors of  
69 future patellofemoral pain include, a decreased peak knee flexion angle, enhanced knee  
70 abduction, decreased vertical ground reaction force, elevated patellofemoral joint reaction  
71 force, and augmented patellofemoral joint stress (16). Similarly, chronic patellar  
72 tendinopathy (or jumper's knee) may account for up to 25 % of all soft tissue injuries, and  
73 forces 53 % of symptomatic athletes to permanently cease physical activities (17).  
74 Biomechanical risk factors linked to the aetiology of patellar tendinopathy include decreased  
75 knee flexion, knee flexion range of motion (ROM), increased patellar tendon force and higher  
76 patellar tendon rate of loading (9, 18).

77

78 Knee braces are commonly utilized in high intensity activities sports such as netball in order  
79 to prevent knee injuries and improve symptoms in those with existing pathologies (19). Knee  
80 braces represent external devices which are designed in order to positively influence the  
81 position of the patella relative to the trochlear groove and improve knee alignment (20). They  
82 range from fixed devices which typically include uniaxial or polyaxial vertical hinges to more  
83 compliant knee sleeves designed to provide knee compression and improve proprioception  
84 (21). Knee braces are a low cost conservative modality that can be utilized during sports  
85 manoeuvres (22). Prophylactic knee braces are designed in order to prevent sportspersons  
86 knee injuries whilst also being minimally restrictive, although there is currently little  
87 published evidence to support their effectiveness in shielding the knee from injury (22).

88

89 The effects of knee bracing have been studied extensively in a range of sports movements.  
90 However, there is currently only one investigation which has examined the effects of knee  
91 bracing in netball players. Sinclair et al., (18) examined the influence of a prophylactic knee

92 brace on patellofemoral joint kinetics and three-dimensional knee joint kinematics during run,  
93 cut and vertical jump movements. Their findings confirmed that there were no differences in  
94 patellofemoral joint kinetics as a function of wearing the knee brace, but knee joint range of  
95 motion in the transverse plane was statistically attenuated. However, there is yet to be any  
96 published information concerning the effects of knee bracing in netball players during single  
97 and double limb deceleration tasks.

98

99 Therefore the aim of the current investigation was to investigate the effects of a prophylactic  
100 knee brace on knee joint kinetics and kinematics during single and double limb deceleration  
101 tasks. The findings may provide both coaches and netballers with information regarding the  
102 utilization of knee bracing for the attenuation of the biomechanical parameters linked to the  
103 aetiology of knee injuries during high intensity netball specific movements.

104

## 105 **Methods**

### 106 *Participants*

107 Twenty female netball players (age =  $19.92 \pm 0.79$  years, height =  $1.66 \pm 0.05$  m, mass =  
108  $62.43 \pm 8.66$  kg) were recruited to for this study. This sample size is commensurate with  
109 previous analyses concerning the effects of prophylactic bracing on knee joint kinetics and  
110 kinematics in netball specific movements (19). Volunteers were considered eligible for  
111 participation if they were; over 18, university first team level players and possessed a  
112 minimum of 3 years of competitive netball experience. Participants were excluded from the  
113 study if there was evidence of existing knee pathology or there had been previous knee

114 **surgery.** Written informed consent was provided and the procedure was approved by the  
115 University.

116

### 117 *Knee Brace*

118 A single nylon/silicone knee brace was utilized in this investigation, (Kuangmi 1 PC  
119 compression knee sleeve), which was worn on the dominant (right) limb in all participants.  
120 The brace examined as part of this study is lightweight knee joint compression sleeve  
121 designed to provide support and enhance joint proprioception.

122

### 123 *Procedure*

124 Participants were required to complete five repetitions of a simulated centre pass movement  
125 (described below), with and without presence of the brace. The order that participants  
126 performed in the movement/ brace conditions was counterbalanced. For the single limb  
127 movement condition, participants were instructed to jog towards the force platform, when  
128 they were within 0.75 m of the plate (marked using masking tape) a regulation size netball  
129 (Gilbert Spectra, Size 5) was passed to them in the opposing direction that they were moving,  
130 by a single university 1st team level netball player. Having caught the ball participants were  
131 required to decelerate by planting their dominant (right) limb on the force platform prior to  
132 the contralateral side. For the double limb condition the process was identical but participants  
133 were required to land with both feet simultaneously, with only the dominant limb on the force  
134 plate. Participants were allowed as much practice time/trials to accommodate to the  
135 experimental conditions as they deemed necessary. To ensure that participants utilized a  
136 similar approach velocity in the brace and no-brace conditions; the linear velocity of the  
137 pelvic segment was quantified. The approach velocity during the first trial in both the single

138 and double limb movement conditions was calculated and a maximum deviation of 5% from  
139 this velocity was allowed throughout data collection for each participant (23). Both  
140 movements were defined as the duration from foot contact (defined as > 20N of vertical force  
141 applied to the force platform), to maximum knee flexion (19).

142

143 In addition to the biomechanical movement information, the effects of the experimental brace  
144 on knee joint proprioception were also examined using a weight bearing joint position sense  
145 test. This was conducted, in accordance with the procedure of Drouin, et al., (24), whereby  
146 participants were assessed on their ability to reproduce a target knee flexion angle of 30°  
147 whilst in single leg stance. To accomplish this, participants were asked to slowly squat to a  
148 knee flexion angle of 30 °, which was verified using a handheld goniometer by the same  
149 researcher throughout data collection. Participants then held this position for 15 seconds  
150 during which time the knee criterion angle was captured using the motion analysis system.  
151 Following this participants were asked to return to a standing position and wait for 15  
152 seconds, and they were required to repeat the above process without guidance via the  
153 goniometer. Again this position was held for a period of 15 seconds and the replication trial  
154 was also collected using the motion analysis system. This above process conducted on three  
155 occasions in both the brace and no-brace conditions in a counterbalanced order, and between  
156 each trial participants walked for 20 ft to eliminate any proprioceptive memory of the  
157 previous trial. The absolute difference in degrees calculated between the criterion and  
158 replication trials was averaged over the three trials to provide an angular error value in both  
159 brace and no-brace conditions, which was extracted for statistical analysis.

160

161 Kinematics and ground reaction force (GRF) information were synchronously collected.

162 Kinematic data were captured at 250 Hz via an eight camera motion analysis system

163 (Qualisys Medical AB, Goteburg, Sweden) and kinetic data using a force platform (Kistler,  
164 Kistler Instruments Ltd., Alton, Hampshire) which operated at 1000 Hz. Dynamic calibration  
165 of the motion capture system was performed before each data collection session. To quantify  
166 lower extremity segments in six degrees of freedom, the calibrated anatomical systems  
167 technique was utilized. To define the anatomical frames of the pelvis, thigh, shank and foot  
168 retroreflective markers (19 mm) were positioned onto the, iliac crest, anterior superior iliac  
169 spine (ASIS), and posterior super iliac spine (PSIS). In addition, further markers were placed  
170 unilaterally onto the, medial and lateral malleoli, greater trochanter, medial and lateral  
171 femoral epicondyles calcaneus, first metatarsal and fifth metatarsal heads of the affected  
172 limb. Carbon-fiber tracking clusters comprising of four non-linear retroreflective markers  
173 were positioned onto the thigh and shank segments. In addition to these the foot segments  
174 were tracked via the calcaneus, first metatarsal and fifth metatarsal, and the pelvic segment  
175 was tracked using the PSIS and ASIS markers. The hip joint centre was determined using a  
176 regression equation, which uses the positions of the ASIS markers and the centers of the  
177 ankle and knee joints were delineated as the mid-point between the malleoli and femoral  
178 epicondyle markers.

179

180 Static calibration trials were obtained with the participant in the anatomical position in order  
181 for the positions of the anatomical markers to be referenced in relation to the tracking  
182 clusters/markers. A static trial was conducted with the participant in the anatomical position  
183 in order for the anatomical positions to be referenced in relation to the tracking markers,  
184 following which those not required for dynamic data were removed. The Z (transverse) axis  
185 was oriented vertically from the distal segment end to the proximal segment end. The Y  
186 (coronal) axis was oriented in the segment from posterior to anterior. Finally, the X (sagittal)

187 axis orientation was determined using the right hand rule and was oriented from medial to  
188 lateral.

189

190 Following completion of the biomechanical data collection, in accordance with Sinclair et al.,  
191 (19); participants were asked to subjectively rate the knee sleeve in relation to performing the  
192 movements without the brace in terms of stability and comfort. This was accomplished using  
193 3 point scales that ranged from 1 = more comfortable, 2 = no-change and 3 = less  
194 comfortable and 1 = more stable, 2 = no-change and 3 = less stable. In addition, each  
195 participant was asked whether they would or would not choose to wear the knee brace during  
196 their training/ competitive netball activities.

197

#### 198 *Data processing*

199 Dynamic trials were digitized using Qualisys Track Manager in order to identify anatomical  
200 and tracking markers then exported as C3D files to Visual 3D (C-Motion, Germantown, MD,  
201 USA). All data were normalized to 100 % of the landing phase. GRF and kinematic data were  
202 smoothed using cut-off frequencies of 50 and 12 Hz with a low-pass Butterworth 4th order  
203 zero lag filter (19). Three dimensional kinematics of the knee and ankle were calculated using  
204 an XYZ cardan sequence of rotations (where X = sagittal plane; Y = coronal plane and Z =  
205 transverse plane). Three dimensional knee joint angular kinematic measures that were  
206 extracted for statistical analysis were 1) angle at footstrike, 2) peak angle and 3) angular  
207 ROM from footstrike to peak angle.

208

209 Patellofemoral loading during the stance phase of running was quantified using a model  
210 adapted from van Eijden et al., (25), in accordance with the protocol of Willson et al., (26). A  
211 drawback of the van Eijden model is that co-contraction of the knee flexor musculature is not  
212 accounted for (26). In order to account for this, we also calculated hamstring and  
213 gastrocnemius forces in accordance with the procedures described by DeVita & Hortobagyi,  
214 (27). To summarize, the hamstring force was calculated using the hip extensor moment,  
215 hamstrings and gluteus maximus cross-sectional areas (28) and by fitting a 2<sup>nd</sup> order  
216 polynomial curve to the data of Nemeth & Ohlsen, (29) who provided muscle moment arms  
217 at the hip as a function of hip flexion angle. The gastrocnemius force was calculated firstly by  
218 quantifying the ankle plantarflexor force, which was resolved by dividing the plantarflexion  
219 moment by the Achilles tendon moment arm. The Achilles tendon moment arm was  
220 calculated by fitting a 2<sup>nd</sup> order polynomial curve to the ankle plantarflexion angle in  
221 accordance with Self & Paine, (30). Plantarflexion force accredited to the gastrocnemius  
222 muscles was calculated via the cross-sectional area of this muscle relative to the triceps surae  
223 (28).

224

225 The hamstring and gastrocnemius forces were multiplied by their estimated muscle moment  
226 arms to the knee joint in relation to the knee flexion angle (31), and then added together to  
227 estimate the knee flexor moment. The derived knee flexor moment was added to the net knee  
228 extensor moment quantified using inverse dynamics were then summed and subsequently  
229 divided by the quadriceps muscle moment arm (25), to obtain quadriceps force adjusted for  
230 co-contraction of the knee flexor musculature. Patellofemoral force was then quantified by  
231 multiplying the adjusted quadriceps force by a constant which was obtained by using the data  
232 of van Eijden et al., (25).

233

234 Finally, patellofemoral joint stress was quantified by dividing the patellofemoral force by the  
235 patellofemoral contact area. Patellofemoral contact areas were obtained by fitting a 2<sup>nd</sup> order  
236 polynomial curve to the sex specific data of Besier et al., (32), who estimated patellofemoral  
237 contact areas as a function of the knee flexion angle using MRI. All patellofemoral forces  
238 were normalized by dividing the net values by bodyweight (BW). From the above processing,  
239 peak patellofemoral force, and peak patellofemoral stress (KPa/BW) were extracted.  
240 Patellofemoral instantaneous load rate (BW/s) was also extracted by obtaining the peak  
241 increase in force between adjacent data points.

242

243 In addition, Patellar tendon loading was quantified using a model similarly adapted from  
244 Janssen et al., (9). Again, the derived knee flexor moment was added to the net knee extensor  
245 moment quantified using inverse dynamics, and then divided by the moment arm of the  
246 patellar tendon, generating the patellar tendon force. The tendon moment arm was quantified  
247 as a function of the sagittal plane knee angle, by fitting a 2<sup>nd</sup> order polynomial curve to the  
248 data provided by Herzog & Read, (33). All patellar tendon forces were normalized by  
249 dividing the net values by bodyweight (BW). From the above processing, peak patellar  
250 tendon force was extracted. Patellar tendon instantaneous load rate (BW/s) was also extracted  
251 by obtaining the peak increase in force between adjacent data points.

252

253 Finally, ACL loading was quantified using the model described previously by Sinclair &  
254 Stainton, (23). All ACL forces were normalized by dividing the net values by bodyweight  
255 (BW). From the above processing, peak ACL force was extracted. ACL instantaneous load

256 rate (BW/s) was also extracted by obtaining the peak increase in force between adjacent data  
257 points.

258

### 259 *Statistical analyses*

260 Descriptive statistics of means and standard deviations were obtained for each outcome  
261 measure. Shapiro-Wilk tests were used to screen the data for normality. Differences in knee  
262 proprioception with and without the presence of the brace were examined using the using a  
263 paired t-test. Differences in biomechanical and knee pain parameters were examined using 2  
264 (BRACE) x 2 (MOVEMENT) repeated measures ANOVA's. Statistical significance was  
265 accepted at the  $P \leq 0.05$  level. Effect sizes for all significant findings were calculated using  
266 partial Eta<sup>2</sup> ( $\eta^2$ ). All statistical actions were conducted using SPSS v24.0 (SPSS Inc,  
267 Chicago, USA).

268

## 269 **Results**

270 Tables 1-3 present the mean  $\pm$  SD knee kinetics and kinematics as a function of different  
271 brace and movement conditions. Figure 1 shows the mean  $\pm$  SD knee proprioception as a  
272 function of wearing the knee brace.

273

### 274 *Patellofemoral loading*

275 A significant main effect of MOVEMENT ( $P < 0.05$ ,  $\eta^2 = 0.43$ ) was noted for peak  
276 patellofemoral load, with the highest forces being experienced in the double limb landing  
277 (Table 1). A significant main effect of movement ( $P < 0.05$ ,  $\eta^2 = 0.41$ ) was also revealed

278 noted for the patellofemoral load rate, with the highest rates of loading being experienced in  
279 the double limb landing (Table 1).

280

### 281 *Patellar tendon loading*

282 No significant ( $P>0.05$ ) differences were observed for patellar tendon loading (Table 1).

283

284 @@@TABLE 1 NEAR HERE@@@

285

### 286 *ACL loading and muscle kinetics*

287 No significant ( $P>0.05$ ) differences were observed for ACL loading (Table 2).

288

289 @@@TABLE 2 NEAR HERE@@@

290

### 291 *Three-dimensional kinematics*

292 In the sagittal plane a significant main effect of MOVEMENT ( $P<0.05$ ,  $p\eta^2 = 0.69$ ) was  
293 noted for the knee flexion angle at footstrike, which was greater in the double limb landing  
294 condition (Table 3). In addition, for peak knee flexion there were significant main effects for  
295 both MOVEMENT ( $P<0.05$ ,  $p\eta^2 = 0.39$ ) and BRACE ( $P<0.05$ ,  $p\eta^2 = 0.62$ ). Peak flexion was  
296 found to be greater in the double limb landing and also in the brace condition (Table 3).  
297 Finally, for sagittal ROM there was a main effects of BRACE ( $P<0.05$ ,  $p\eta^2 = 0.37$ ), which  
298 was found to be greater in the brace condition (Table 3).

299

300 In the coronal plane a significant main effect of MOVEMENT ( $P < 0.05$ ,  $\eta^2 = 0.36$ ) was  
301 noted for the knee abduction angle at footstrike, which was greater in the double limb landing  
302 condition (Table 3). In addition there was also a main effect of MOVEMENT ( $P < 0.05$ ,  $\eta^2 =$   
303  $0.37$ ), for the peak knee abduction angle, which was shown to be greater in the double leg  
304 landing condition (Table 3). Finally, for coronal plane ROM there was a main effects of  
305 movement ( $P < 0.05$ ,  $\eta^2 = 0.48$ ), which was found to be greater in the double leg landing  
306 condition (Table 3).

307

308 In the transverse plane a significant main effect of BRACE ( $P < 0.05$ ,  $\eta^2 = 0.37$ ), was noted  
309 for the knee external rotation angle at footstrike, which was significantly lower in the brace  
310 condition (Table 3).

311

312 @@@TABLE 3 NEAR HERE@@@

313

314 *Knee proprioception*

315 No significant ( $P = 0.44$ ) differences in knee proprioception were observed.

316

317 @@@FIGURE 1 NEAR HERE@@@

318

319 *Subjective ratings*

320 Subjective ratings of comfort showed no significant changes were found when wearing the  
321 knee braces ( $X^2=0.70, P=0.40$ ), with 5 participants rating the brace as more comfortable, 7 no  
322 change and 8 less comfortable. However, participants subjectively rated that wearing the knee  
323 brace significantly increased stability during both landings ( $X^2= 14.80, P<0.001$ ), with 14  
324 participants rating the brace as more stable, 6 no change and 0 less stable. Finally, no  
325 significant change was observed for participants subjective indication of whether they would  
326 choose to wear the brace ( $X^2= 1.80, P=0.18$ ), with 7 participants indicating that they would  
327 wear the brace for their netball training/ competition activities and 13 indicating that they  
328 would not.

329

## 330 Discussion

331 To the authors knowledge this represents the first investigation to explore the influence of  
332 prophylactic knee bracing during netball specific deceleration tasks and thus may provide  
333 important information to netballers and clinicians regarding the efficacy of knee bracing in  
334 this sporting discipline. The findings from this study show that whilst participants perceived  
335 that the brace significantly improved joint stability, the presence of the brace did not mediate  
336 any significant alterations in the kinetic/ kinematic parameters linked to the aetiology of  
337 injury.

338

339 The current investigation showed firstly that neither ACL, patellofemoral or patellar tendon  
340 loading were statistically influenced as a function of the knee brace condition. This  
341 observation is in agreement with those of Sinclair et al., (19) who showed that knee bracing  
342 did not significantly affect patellofemoral loading during netball specific movements,

343 although it should be noted that neither ACL or patellar tendon kinetics were examined in  
344 this study. As the current study utilized a lightweight nylon/ silicone construction, it is  
345 proposed that this observation relates to the mechanical structure of the knee brace which was  
346 not able to provide sufficient physical restraint to mediate alterations in knee joint loading.  
347 Nonetheless excessive loading at the ACL, patellofemoral joint and patellar tendon are  
348 considered to be one of the key mechanisms linked to the aetiology of knee pathologies in  
349 athletic populations (9, 12, 16). Therefore the key implication from this observation is that  
350 the prophylactic brace examined in this study does not appear to reduce the knee kinetic  
351 parameters that have been linked to the aetiology of knee pathologies in netball specific  
352 single and double limb deceleration tasks.

353

354 It has been proposed that knee bracing facilitates safer movement mechanics during dynamic  
355 activities, by promoting an enhanced perception of joint stability (34). The subjective ratings  
356 of stability noted in the current investigation support this notion in that participants perceived  
357 that the knee brace significantly improved knee joint stability. However, the current  
358 investigation also showed that knee proprioception was not statistically improved as a  
359 function of wearing the prophylactic knee brace. This indicates that the perceived change in  
360 stability was not apparent in either the deceleration movements or the proprioceptive task.  
361 Proprioceptive acuteness, an element of the sensorimotor system, is reflective of an athlete's  
362 ability to perceive joint position, motion and external forces in order to differentiate lower  
363 limb movement (35). As such, improving knee joint proprioception acuity is considered an  
364 essential component for injury prevention as it makes the knee joint more receptive to  
365 potentially injurious forces (36).

366

367 The observations from this investigation concur with those of Bottoni, et al., (37) yet disagree  
368 with the observations of Birmingham et al., (38), Herrington et al., (34) and Van Tiggelen et  
369 al., (39). The lack of agreement between studies in general is due to the lack of  
370 standardization of testing protocols to quantify knee joint proprioception (33). However, the  
371 current investigation selected a weight bearing joint position sense protocol based on the  
372 notion proposed by Hanafy, (40), that this technique provides more clinical and ecological  
373 relevance when evaluating proprioception in relation to weight bearing specific pathologies.  
374 Nonetheless the current investigation has demonstrated that prophylactic knee bracing does  
375 not improve knee joint proprioception in a weight bearing angle reproduction test in netball  
376 players. The proposed mechanism by which knee bracing is considered to enhance joint  
377 proprioception is through compression of the skin/ musculature, which serves to stimulate  
378 sense receptors and increase the afferent input from the joint surrounding structures (34).  
379 Thus it can be speculated that the brace may not have provided sufficient compression to the  
380 knee to mediate statistical improvements in joint proprioception. Further research into the  
381 association between compression provided by the knee brace and joint proprioception is thus  
382 a clear avenue for further investigation.

383

384 A potential limitation to this work is that joint kinetics were obtained using a musculoskeletal  
385 modelling approach as opposed to an in vivo exploration of knee loading. This process was  
386 necessary due to the impracticalities and invasive nature of obtaining direct kinetic  
387 measurements. However, although this approach represents expansion compared to previous  
388 mechanisms in that co-contraction of the knee flexor musculature was accounted for, further  
389 work is required to improve the efficacy of subject specific knee joint musculoskeletal  
390 models which will make possible further developments in clinical biomechanics. In addition,  
391 a further potential limitation of the current investigation is that it examines healthy netballers

392 who did not habitually wear knee bracing. This means that the findings are not generalizable  
393 to netballers with existing knee joint pathology. Future, prospective analyses will help to  
394 determine the clinical efficacy of knee braces as treatment modalities for netballers with  
395 existing knee injuries.

396

## 397 **Conclusion**

398 This study showed firstly that neither ACL, patellofemoral nor patellar tendon kinetic  
399 parameters were significantly affected as a function of the knee brace. The findings did show  
400 however that the knee brace helped to increase perceived knee stability, but there were no  
401 statistical improvements in weight bearing knee proprioception. This indicates that the  
402 perceived change in stability was not apparent in either the deceleration movements or  
403 proprioceptive tasks. The current investigation indicates that the utilization of prophylactic  
404 knee bracing akin to the device used in the current study, does not appear to reduce the  
405 biomechanical parameters linked to the aetiology of knee injuries, during netball specific  
406 deceleration movements. However, further prospective analyses are required to fully  
407 substantiate this proposition.

408

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411

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529 **Tables**

530 **Table 1: Mean ± SD patellofemoral and patellar tendon kinetics as a function of the knee**  
 531 **brace and different movement conditions.**

	No-brace				Brace				P-value		
	Single		Double		Single		Double		BRACE	MOVEMENT	BRACE * MOVEMENT
	Mean	SD	Mean	SD	Mean	SD	Mean	SD			
Peak patellofemoral force (BW)	3.99	0.98	4.63	1.33	4.21	1.57	4.93	1.37	0.20	0.02	0.84
Peak patellofemoral stress (KPa/BW)	15.12	2.82	15.21	3.85	15.15	4.35	16.11	3.43	0.42	0.39	0.50
Patellofemoral load rate (BW/s)	119.82	24.76	144.11	50.96	108.82	36.34	137.08	42.55	0.21	0.02	0.80
Peak patellar tendon force (BW)	6.07	1.23	6.14	1.56	6.17	1.75	6.49	1.42	0.49	0.32	0.63
Patellar tendon load rate (BW/s)	246.31	50.38	281.14	92.09	219.89	77.69	263.19	81.68	0.07	0.14	0.75

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533

534 **Table 2: Mean ± SD ACL kinetics as a function of the knee brace and different movement**  
 535 **conditions.**

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	No-brace				Brace				P-value		
	Single		Double		Single		Double		BRACE	MOVEMENT	BRACE * MOVEMENT
	Mean	SD	Mean	SD	Mean	SD	Mean	SD			
Peak ACL force (BW)	1.19	0.38	1.29	0.31	1.30	0.39	1.30	0.37	0.51	0.52	0.56
ACL load rate (BW/s)	113.59	51.69	115.04	53.56	131.49	57.53	106.12	35.03	0.11	0.69	0.12

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545 Table 3: Mean  $\pm$  SD knee joint kinematics as a function of the knee brace and different  
 546 movement conditions.

	No-brace				Brace				P-value		
	Single		Double		Single		Double				
	Mean	SD	Mean	SD	Mean	SD	Mean	SD	BRACE	MOVEMENT	BRACE * MOVEMENT
<b>Sagittal plane (positive = flexion)</b>											
Angle at footstrike (°)	16.35	3.73	20.54	5.14	17.70	4.77	22.18	6.85	<0.001	0.11	0.80
Peak flexion (°)	60.37	7.43	69.91	8.82	65.30	9.21	72.72	11.29	0.02	0.001	0.37
ROM (°)	44.02	6.72	49.37	9.02	47.60	9.08	50.54	9.39	0.17	0.03	0.35
<b>Coronal plane (positive = abduction)</b>											
Angle at footstrike (°)	0.93	4.08	0.64	4.31	1.92	3.82	0.89	3.48	0.04	0.34	0.11
Peak abduction (°)	5.20	7.26	8.64	8.22	7.02	8.10	9.42	7.63	0.03	0.29	0.38
ROM (°)	4.27	4.00	8.00	5.63	5.10	5.79	8.53	5.52	0.009	0.56	0.80
<b>Transverse plane (positive = external rotation)</b>											
Angle at footstrike (°)	9.57	11.71	8.83	8.47	6.05	10.41	6.24	9.57	0.81	0.03	0.56
Peak external rotation (°)	-4.67	8.53	-5.66	6.79	-6.90	8.87	-7.13	6.81	0.49	0.08	0.28
ROM (°)	14.25	4.50	14.49	4.35	12.95	5.22	13.36	6.24	0.73	0.33	0.91

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549 **Figure labels**

550 Figure 1: Mean  $\pm$  SD angular error values for both brace and no-brace conditions during the  
 551 weight bearing joint position sense test.