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2 during gait?
3

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11

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- 20 Brief Title: Does orthotic walker boot design influence biomechanics during gait?

22 Abstract

23 Background: Undesirable lower limb gait deviations have previously been reported when wearing orthotic walker boots, therefore there is a need to optimise orthotic walker boot designs 24 25 to facilitate normal gait. Objective: This study explored the biomechanical effects of two designs 26 of orthotic walker boot on the lower limb and trunk compared to usual footwear. Study Design: 27 A repeated measures analysis of variance (ANOVA) was used to evaluate selected kinematic and 28 kinetic variables under different walking conditions. Methods: Sixteen healthy participants 29 walked in three conditions using: Walker A (Airselect Elite, Enovis, USA), Walker B (Townsend 30 XLR8 Series Walker, Thuasne, France) and a usual shoe. A 10 camera motion analysis system 31 and 4 force plates were used to collect kinematic and kinetic data. Results: Gait speed was 32 significantly slower in both orthotic walker boots, and significantly decreased ankle range of 33 motion (ROM) which is their primary function. Significant deviations in normal knee and hip 34 kinematics and kinetics, shank to vertical angle and pelvic and trunk movements were noted with 35 both walker boots, with the greatest deviations from the shoe condition observed in Walker B. 36 Recline and incline shank angular velocities showed the greatest differences in Walker B which 37 could be associated with adverse knee joint moments and a significantly greater perceived ease 38 of walking in Walker A. Conclusions: Orthotic walker boot design significantly affects walking 39 mechanics. Orthotic walkers with greater forefoot rocker profiles and inclined vertical shank 40 angles may at least in part mitigate known gait deviations when wearing orthotic walkers.

41

42 Keywords: Gait, Lower limb Orthoses, Joint Mechanics, Rehabilitation, Rocker Sole Profile,
43 Shank to Vertical Angle (SVA).

45 Background & Aims

Orthotic walker boots are included in clinical practice during the management of 46 foot/ankle fractures ¹, severe ankle sprains ¹, chronic tendinopathy, ² post-surgical 47 stabilization ^{1,2}, and in the prevention/treatment of ulceration in individuals with diabetes. 48 ^{3,4} The advantages of using an orthotic walker boot are multifaceted. ^{1,2,4} They allow early 49 weight bearing whilst still providing protection, provide effective oedema management, 50 and reduce the biomechanical adverse effects on gait patterns compared to a synthetic 51 walking cast, whilst also allowing removal for rehabilitation, examination and cleaning. 52 ^{1,2,4} Improved clinical outcomes have been reported with orthotic walker boots, with early 53 54 mobilization leading to improved ankle joint function, bone strength and faster bone healing. ¹ Shorter hospital stays and fewer rehabilitation sessions have also been 55 56 associated with the cost-effectiveness of using orthotic walker boots over traditional casting methods. 1,2,5 57

58

Orthotic walker boot treatment times can vary from between one and three months, depending upon injury severity or the clinical needs of the patient. ⁶ Throughout this time, the individual may adopt an altered gait pattern, with undesirable changes to lower limb kinematics and kinetics, which over time, may result in the development of secondary pain. ⁶ Biomechanical investigations into the effects of orthotic walkers during walking have identified significant, unfavourable effects on knee and hip joint angles and moments. ^{2,4} Different shank to vertical angles (SVA) or tibial inclination angles ⁷ and
heel, midfoot and forefoot rocker profiles have all been suggested to influence gait
patterns to varying extents in different patient groups. ⁸

68

Millions of orthotic walkers are sold globally each year, and although the clinical 69 outcomes are well documented ^{9–11}, limited evidence exists on the effect of these devices 70 on lower limb and trunk kinematics. To improve the biomechanics and ease of walking, 71 changes in the design of orthotic walkers have recently been observed, with greater 72 consideration given to SVAs and rocker profiles.⁴ However, to the authors' knowledge, 73 74 no studies have explored the effects that specific SVA and rocker profile design changes may have on lower limb joint biomechanics to determine how to optimise gait whilst still 75 76 eliciting the positive clinical outcomes already associated with these devices'. This study 77 aimed to explore the biomechanical and subjective effects of a new design of orthotic walker boot compared to a walker with an existing design, to explore whether design 78 changes have gone some way to normalising gait patterns. 79

80

81 Methods

82 Design

A within subjects, repeated measures design was used to analyse changes in gait
parameters under three conditions.

86 *Participants*

Healthy participants without current musculoskeletal injuries or disorders, a 87 history of surgery or traumatic injury to the lower extremities or lower back, and no 88 89 history of medical conditions that limit physical activity were recruited from university populations. Previous knee extension moment⁴ was used to determine sample size and a 90 minimum of ten participants was required. Data collection conformed to the Declaration 91 of Helsinki¹² and volunteers provided written informed consent prior to participation. 92 The study was approved by the University's Health Ethics Review Panel (reference 93 94 HEALTH 0258).

95

96 *Procedure*

97 Passive retro-reflective markers were placed on the lower limbs and pelvis using the calibrated anatomical system technique, and segmental kinematics were tracked in 6 98 degrees of freedom. ¹³ Markers were placed on the acromions, anterior and posterior 99 superior iliac spines, greater trochanters, medial and lateral femoral epicondyles, medial 100 and lateral malleoli, the head of the 1st and 5th metatarsals, the dorsum of the foot and the 101 calcaneus, and the equivalent placement over these landmarks on the orthotic walkers. 102 Clusters of four non-collinear markers were attached to the body segments of the shank 103 and thigh and on the anterior plate of the walker.⁴ Kinematic data were collected at 100Hz 104

using a 10-camera infrared Oqus motion analysis system (Qualisys Medical AB,
Sweden), and kinetic data were collected at 200Hz using four AMTI force plates (Boston,
MA, USA).

108

109 All participants walked along a 10m walkway under three conditions: participant's own footwear (shoe); Walker A (Airselect Elite, Enovis, USA) and Walker 110 B (Townsend XLR8 Series Walker, Thuasne, France), with the orthotic walkers worn on 111 112 the right leg and the participant's own shoe on the left (Figure 1). Walker A was included as the significant design changes to the rocker profile and SVA angle warrant comparison 113 114 against current practice, and Walker B was selected as the comparator, due to its widespread use across multiple healthcare systems. Walker A is characterised by a 115 116 forefoot rocker profile of twelve degrees and a vertical shank angle of four degree 117 (inclined). Walker B is characterised by a shallower forefoot angle (6 degrees) and a 118 vertical shank angle of zero degrees (vertically upright). Boot conditions were worn in randomised order (http://www.randomization.com). Both orthotic walkers were applied 119 120 as per manufacturer's guidance, including air cell inflation Five repetitions where the participant's right foot landed within the perimeter of a force plate were recorded per 121 condition. Upon completion of the walking tasks, participants rated their perceived ease 122 of walking in both orthotic walker boot conditions on a numerical scale of 0 'very 123 difficult' to 10 'very easy'. 124

126

Data Processing and Analysis

Anatomical frames were defined by landmarks positioned at the medial and lateral 127 borders of the joint, from these right-handed segment co-ordinate systems were defined. 128 129 The kinematics were calculated based on the Cardan sequence of XYZ equivalent to the joint coordinate system.¹⁴ Raw kinematic and kinetic data were exported to Visual3D 130 (C-Motion Inc, USA) and filtered using fourth order Butterworth filters with cut-off 131 frequencies of 6 and 25Hz respectively. Gait speed was calculated from the time and 132 distance between consecutive right heel strikes with the first heel strike being on a force 133 134 platform. Ankle, knee, hip, pelvis and trunk (defined as left and right acromions and posterior superior iliac spines) angles and external moments were exported and the 135 136 maximum, minimum and range of motion (ROM) at key events (heel strike, stance phase, 137 swing phase, full gait cycle) were found. Given the specific design differences in Walker Boots relating to the vertical angle, SVA was included. It was calculated as the angle of 138 the right shank relative to the laboratory coordinate system and the minimum (maximum 139 140 tibial recline angle), maximum (maximum tibial incline angle) and SVA ROM were all reported.⁷ Shank angular velocity was calculated as a first derivative of the tibial angle 141 142 during the stance phase of the gait cycle.

143

The data distribution for each variable was tested using Kolmogorov-Smirnov tests. For normally distributed data Repeated Measures Analysis of Variance (ANOVA) 144

145	tests were performed using SPSS v28 (IBM, NY, USA), and mean, standard deviations,
146	main effects and effect sizes were reported (Table 1 and 2). Where a main effect was seen
147	Least Significant Difference post-hoc pairwise comparisons were performed (Table 3).
148	Where the data were not normally distributed Friedman and Wilcoxon signed rank tests
149	were performed. The level of significance was set at $p < 0.05$ throughout.
150	
151	Results
152	Sixteen healthy participants (10 males, 6 females), with a mean age 30 ± 5.7 years,
153	height 1.73 ± 0.1 m and mass 79.7 ± 15.5 kg were included.
154	
155	Gait parameters
156	A significant main effect was seen for gait speed (p<0.001, range 1.23–1.37 m/s).
157	Post-hoc comparisons demonstrated that gait speed was significantly reduced in Walker
158	A (p<0.001) and Walker B (p<0.001) compared to the shoe, but there was no significant
159	difference between walkers (p=0.267).
160	
161	Kinematics
4.60	

162 At the ankle significant main effects were seen during stance and swing phase 163 (p<0.001). Post-hoc comparisons showed that both orthotic walker boots performed 164 comparably with no significant differences, however notable differences were seen between the Walkers and the shoe (p<0.001). Both Walker A and B significantly decreased ankle plantarflexion angle during stance (p<0.001) and swing phase (p<0.001) and significantly increased dorsiflexion angle during mid-stance (p<0.001).

168

169 At the knee significant main effects were seen at heel strike (p<0.001) and during 170 swing phase (p=0.008), for knee valgus angle (p<0.001), and transverse plane ROM (p=0.038). Post-hoc comparisons showed that both Walker A and B significantly 171 172 increased knee flexion angle at heel strike and during stance phase compared to the shoe (p<0.031). Walker B had a significantly greater effect on knee flexion angle at heel strike 173 174 and during stance phase compared to Walker A (p<0.033). During the swing phase, significant differences were seen in knee flexion angle, with Walker A reducing knee 175 176 flexion compared to the shoe and Walker B (p<0.014). Walker B had no effect on knee 177 flexion during the swing phase compared to the shoe (p=0.246). Both Walker A and B 178 significantly reduced knee valgum compared to the shoe condition (p=0.003).

179

At the hip significant main effects were seen during the gait cycle (p<0.041). Posthoc comparisons showed that both Walker A and B significantly reduced hip adduction angle, internal rotation and coronal plane ROM compared to the shoe (p<0.005). Walker B significantly increased sagittal plane ROM compared to the shoe (p=0.003).

Both Walker A and B significantly reduced coronal plane pelvic ROM compared to the shoe (p < 0.009). Walker A also significantly reduced pelvic obliquity compared to 185 the shoe (p<0.014). Walker A and B significantly increased trunk sagittal plane ROM 186 compared to the shoe (p < 0.006). 187

188

For the SVA, significant main effects were seen for maximum tibial recline angle 189 (p<0.001), tibial inclination angle (p<0.001) and SVA range (p<0.001). Post-hoc 190 191 comparisons showed that during early stance phase, the maximum tibial recline angle was 192 significantly different between all conditions, with Walker A and B demonstrating 193 significantly lower recline angles than the shoe (p=0.014, p=0.001) respectively, with Walker B having a significantly lower recline angle than Walker A (p=0.012). Both 194 195 Walker A and B significantly reduced the maximum tibial inclination angle during late 196 stance phase compared to the shoe (p=0.001, p=0.026) respectively, with no differences 197 seen between Walkers. Similarly, for SVA ROM during stance phase, both Walker A and B showed significantly lower ROM compared to the shoe (p=0.001, p<0.001)198 199 respectively, with no differences seen between Walkers. For shank angular velocity, 200 significant main effects were seen during early (p=0.010) and late (p<0.001) stance phase. 201 During early stance phase post-hoc comparisons showed that the angular velocity was significantly greater in Walker B compared to Walker A (p=0.015) and the shoe 202 203 (p<0.001), with no differences seen between Walker A and the shoe. During late stance

phase, similar differences were noted, with Walker B demonstrating significantly greater peak angular velocities compared to Walker A (p=0.003) and the shoe (p<0.001), again with no differences seen between Walker A and shoe.

207

208 Joint Moments

209 Significant differences in knee extension moments after heel strike were seen between the shoe and the Walkers, with both Walkers demonstrating significantly 210 211 reduced knee extension moments at heel strike (p<0.005). Walker A also demonstrated a 212 significantly reduced knee extension moment compared to Walker B at heel strike 213 (p=0.050). Significant main effects were noted in the peak flexion moments during mid 214 stance phase (p=0.004). The knee flexion moment during mid stance was significantly 215 greater with Walker B compared to the shoe (p=0.010), and Walker A (p=0.006), with no 216 differences seen between the shoe and Walker A (p=0.240).

217

During late stance phase significant main effects were seen (p<0.001) in peak extension moments. Walker B had a significantly greater peak extension moment compared to the shoe (p=0.001) and Walker A (p=0.019), with a trend towards a significant difference between the shoe and Walker A (p=0.053). Significant main effects were also noted in peak adduction moments (p<0.001), with significant reductions observed in Walker B compared to the shoe (p=0.009) and Walker A (p=0.015).

Significant differences were seen in hip peak adduction moments and rotation moments (p<0.022) between Walker B and the shoe (p=0.009) with Walker B showing greater moments, whereas no significant differences were seen between the shoe and Walker A (p=0.141).

229

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230 Perceptions
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Participants perceived that Walker A was significantly easier to walk in compared
to Walker B (p=0.044), with median scores of 6.5 (range 4.0 – 10.0) and 6.0 (range 4.08.0) out of ten, respectively.

234

235 Discussion

236 This study aimed to explore how different designs of orthotic walker boots affect gait in healthy participants. The need for further research to identify how to optimise gait 237 whilst wearing orthotic walker boots has been highlighted. ^{6,15} Previous work has 238 identified that SVAs ⁷ and rocker profiles can significantly influence gait patterns to 239 different extents. ⁴ Specifically relevant to the rocker profiles, the apex position and angle, 240 241 and rocker radius can influence the plantar pressure redistribution and lower limb kinetics and kinematics whilst walking when wearing rocker profile shoes, ¹⁶ with smaller rocker 242 radii reducing dorsiflexion and plantarflexion moments at the ankle ¹⁷, which have been 243

considered in the design of orthotic footwear. It is also important to consider these factorsin the design of an orthotic walker.

246

In this study, both orthotic walker boots significantly reduced gait speed compared 247 248 to the shoe, and displayed comparable effects at the ankle, intentionally blocking sagittal plane movement compared to normal walking. Given that an orthotic walker boot's 249 primary function of is relieve and protect affected tissues by limiting ROM at the ankle 250 joint, ¹⁸ both walker boots were shown to perform this function to a similar effect, 251 252 suggesting that the design differences between walker boots does not influence primary 253 function. Biomechanical assessment of remaining lower limb joints may assist in determining whether the different designs of walker boots alter walking patterns to 254 255 different extents.

256

At the knee, deviations in normal movement were seen during the loading phase, with increased knee flexion when wearing both orthotic walker boots. Similar findings have been noted previously ^{2,4,19} and could be associated with the compensation needed due to restricted ankle movement. Results from this study indicate deviations in normal knee movement when wearing both orthotic walker boots, with the greatest deviations observed in Walker B. Walker B, which incorporated a shallower forefoot rocker profile angle, had a significantly greater effect on knee flexion during the loading phase 264 compared to Walker A. During swing phase Walker A also showed less knee flexion compared to Walker B and the shoe possibly indicating that less knee flexion was required 265 to ensure toe clearance. The aim of a forefoot rocker is to enable "rocking" from heel-266 strike to toe-off, facilitating a more 'normal' gait ^{19,20}. This study's results indicate that 267 268 the specific design of the forefoot rocker profile may affect the extent deviation from normal walking, with a shallower rocker profile affecting an individual's ability to 'rock' 269 more than a forefoot rocker profile with a greater angle. A forefoot rocker profile is 270 271 proposed to aid forward progression of the tibia and facilitate tibial shank advancement when sagittal plane ankle movement is restricted.⁸ This study's findings suggest a greater 272 273 forefoot rocker profile angle limits deviations from normal gait kinematics. Much less work has considered the effect of heel rockers on gait kinematics, ²¹ although the 274 275 consensus is that the heel rocker predominantly affects the ankle joint and has a lesser affect proximally. ^{21–23} 276

277

Orthotic walker boots have been shown to affect joint loading at the knee, with greater knee extensor moments observed in the late stance phase in walker conditions compared to a no walker condition. ^{2,4} In the current study significant decreases in knee extension moments after heel strike were observed in both walker boots, suggesting reduced loading through the knee initially. These reduced extension moments may be associated with reduced loads and may be attributed to the differences in the rocker profiles and SVA between conditions. During the loading phase however, Walker B significantly increased the knee flexion moment (mid-stance phase) and knee extension moment (late-stance phase) compared to Walker A and the shoe, indicating greater deviation from normal walking.

288 This study also considered the peak SVA which showed that both Walkers had a lower SVA during early and late stance phase, with Walker B showing the greatest 289 deviation. During the stance phase of a normal gait cycle, the shank transitions from a 290 reclined position in early stance phase to an inclined position at late stance phase.⁷ 291 292 Considering the differences between Walkers, Walker B has both a shallower forefoot 293 rocker profile, and a more upright SVA, and these design specifications may prohibit normal shank movement throughout the stance phase compared to the greater forefoot 294 295 rocker profile and inclined vertical angle of Walker A.

296

This study also considered the use of shank angular velocity to understand movement control from the reclined position to the inclined position. Although both Walkers had similar differences in the SVA ranges of motion compared to the shoe, the shank angular velocity indicated that Walker A showed a greater similarity to the shoe, with no significant differences in the recline and incline shank peak velocity. When considering the significantly greater knee extension moments observed during late stance phase in Walker B only, the differences in the control of the forward progression of the shank could be responsible for these differences. This would suggest that the increased
loading at the knee into hyperextension is associated with the increase in the speed of
shank progression seen in Walker B. As these differences were not observed in Walker
A, this indicates that significant gait deviations may be mitigated with careful
consideration of the SVA and rocker profiles within orthotic walker boot design.

309

Adaptations at the hip were required to afford walking in both orthotic walker 310 311 boots, with the most significant findings observed in the coronal and transverse planes. Regardless of walker boot condition, there was significantly less coronal plane hip 312 313 movement, and a more externally rotated hip was observed compared to normal walking, with Walker B showing greatest deviation. Similar findings have been reported 314 315 previously, with orthotic walker boots reducing hip abduction ROM compared to a shoe condition.² Significant differences were also identified between standardised footwear 316 and orthotic walkers in the transverse plane during stance phase. ⁴ Walker B also 317 significantly increased the hip ROM in the sagittal plane compared to the shoe, and 318 319 increased the peak adduction joint moments compared to the shoe and Walker A, overall 320 demonstrating that greater gait adaptations and potentially greater work done by the muscles were required with Walker B. The pelvis and trunk data findings suggest that 321 whilst the walker boots had an effect on pelvic and trunk mechanics during walking, the 322 design differences between boots did not elicit any significant differences. 323

When considering the ease of walking, Walker A was shown to be significantly easier to walk in compared to Walker B, indicating that the biomechanical differences measured between the two walkers may be associated with a statistically important difference in user experience, however the difference in user experience observed in this study did not reach the threshold for a minimal clinical important change.

330

Although pertinent findings are presented within this study, it is not without its 331 limitations. This research may be considered more valuable had the participant sample 332 included patients with a relevant pathology. However, it is important to understand the 333 334 effects of an intervention amongst a healthy population prior to investigation amongst a 335 pathological group. Both of the walker boots included in this study had air cells to assist 336 immobilisation of the foot and ankle and prevent tibial movement within the boot. 337 Considering participant burden and acceptable data collection session times, the pressure 338 of these air cells was not objectively measured or controlled in this study, although they were inflated in accordance with manufacturers' guidance. To strengthen any future 339 studies, recording pressure values within the walker boot to standardise the pressure 340 applied across participants may be beneficial. Another similar limitation is that the plantar 341 342 pressures were not measured during this study, and therefore the effect of the design 343 changes and materials of the insole and sole of the walker boots remains unknown. Future studies could incorporate plantar pressure to consider this effect. 344

346 Conclusion

The results of this study suggest that Walker B required greater gait adaptations compared to Walker A. As hypothesised, specific designs of walker boot have a significant effect on walking mechanics and may have detrimental effects when worn for a period of time. The findings from this study suggest that significant gait deviations may at least in part be mitigated with careful consideration of the SVA and rocker profiles within an orthotic walker boot design with a greater forefoot rocker profile and an inclined SVA facilitating more 'normal' walking patterns.

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422 Figure Captions

- 423 Figure 1: A Aircast® Airselect Elite (Walker A) with a vertical inclination angle of 4°
- and forefoot rocker profile 12°, and B XLR8 Series Walker (Walker B) with a tibial
 inclination angle of 0° (vertically upright) and forefoot rocker profile 6°
- 426

427 Table Captions

- 428 Table 1: Mean (SD), main effects and effect sizes for kinematic variables. Significance 429 level p < 0.05. * denotes significance.
- 430
- 431 Table 2: Mean (SD), main effects and effect sizes for kinetic variables (Nm/kg).
- 432 Significance level p<0.05. * denotes significance.
- 433
- Table 3: Mean difference, post-hoc pairwise comparisons and 95% confidence intervals
- for ankle, knee, hip, pelvis & trunk kinematics. Significance level p<0.05.* denotes
 significance.
- 437

438 Figures



439

Figure 1: A - Aircast® Airselect Elite (Walker A) with a tibial inclination angle of 4° and
forefoot rocker profile 12°, and B - XLR8 Series Walker (Walker B) with a tibial
inclination angle of 0° (vertically upright) and forefoot rocker profile 6°

		WA	WB	S	p value	Effect Size
Gait speed (m/s)		1.24 (0.15)	1.23 (0.17)	1.37 (0.12)	<0.001*	0.659
SVA (°)	Maximum tibial recline angle	-16.01 (2.51)	-14.23 (2.39)	-18.21 (3.79)	< 0.001*	0.452
	Maximum tibial inclination angle	50.50 (2.57)	51.55 (3.49)	53.26 (2.66)	< 0.001*	0.372
	Range	66.51 (3.77)	65.77 (5.22)	71.47 (3.36)	< 0.001*	0.502
Shank Angular	Peak during early stance phase	165.78 (49.65)	184.94 (31.43)	154.33 (19.52)	0.010*	0.318
Velocity (°/s)	Peak during late stance phase	222.86 (24.41)	251.10 (34.45)	200.91 (24.41)	< 0.001*	0.485
Ankle	Sagittal plane angle at heel strike	7.68 (2.12)	8.02 (1.65)	6.84 (3.45)	0.385	0.062
Kinematics (°)	Plantarflexion angle during stance phase	7.08 (2.12)	7.27 (1.76)	-2.54 (2.84)	< 0.001*	0.894
	Dorsi flexion angle during stance phase	11.54 (3.26)	11.88 (2.40)	17.55 (3.38)	< 0.001*	0.711
	Plantar flexion angle during swing phase	6.329 (2.50)	7.00 (1.74)	-11.48 (6.34)	< 0.001*	0.884
Knee	Sagittal plane angle at heel strike	8.017 (3.84)	9.51 (5.38)	5.40 (4.59)	< 0.001*	0.462
Kinematics (°)	Flexion angle during stance phase	22.76 (5.68)	25.48 (5.86)	20.38 (6.27)	<0.001*	0.522
	Extension angle during stance phase	7.990(6.98)	6.483 (6.26)	7.95 (6.15)	0.141	0.122
	Flexion angle during swing phase	64.63 (6.11)	67.04 (5.64)	68.59 (5.15)	0.008*	0.274
	Maximum valgus angle	0.99 (2.29)	1.03 (2.11)	2.32 (2.48)	0.001*	0.364
	Maximum varus angle	-5.74 (3.15)	-5.68 (2.90)	-4.42 (4.54)	0.096	0.159
	Coronal plane ROM	-6.73 (2.38)	-6.71 (2.32)	-6.74 (3.30)	0.991	0.000
	Internal rotation angle	7.08 (7.08)	7.11 (7.73)	3.77 (7.22)	0.081	0.154
	External rotation angle	-10.53 (8.33)	-9.98 (8.93)	-10.17 (7.06)	0.889	0.004
	Transverse plane ROM	17.61 (5.71)	17.09 (5.72)	13.93 (4.90)	0.038*	0.196
Нір	Flexion angle	40.69 (9.64)	39.57 (10.72)	38.66 (10.00)	0.172	0.111
Kinematics (°)	Extension angle	0.49 (11.61)	-1.12 (11.62)	0.02 (10.80)	0.107	0.138
	Sagittal plane ROM	40.20 (4.93)	40.70 (4.77)	38.64 (3.97)	0.044	0.209
	Abduction angle	5.71 (2.46)	5.11 (3.37)	5.42 (3.01)	0.645	0.029
	Adduction angle	-6.11 (3.24)	-6.61 (2.71)	-9.16 (3.23)	< 0.001*	0.446
	Coronal plane ROM	11.83 (2.87)	11.72 (3.00)	14.57 (3.18)	< 0.001*	0.574
	External rotation angle	3.40 (10.80)	3.85 (11.07)	2.34 (10.69)	0.171	0.111
	Internal rotation angle	-8.11 (9.55)	-7.46 (9.75)	-10.18 (9.90)	0.005*	0.297
	Transverse plane ROM	11.50 (4.65)	11.31 (4.35)	12.52 (4.29)	0.041*	0.192
Pelvis	Maximum anterior pelvic tilt	18.37 (8.50)	17.526 (8.89)	16.63 (8.70)	0.079	0.156
Kinematics (°)	Minimum anterior pelvic tilt	15.04 (8.50)	13.68 (9.15)	13.36 (8.71)	0.103	0.140
	Sagittal plane ROM	3.33 (1.18)	3.849 (1.89)	3.27 (1.18)	0.103	0.140
	Maximum Downwards Pelvic Obliquity	-3.78 (2.31)	-2.98 (2.14)	-3.65 (2.19)	0.204	1.00

444 Table 3: Mean (SD), main effects and effect sizes for kinematic variables. Significance level p < 0.05. * denotes significance.

	Maximum Upwards Pelvic Obliquity	3.90 (2.79)	4.51 (3.12)	5.35 (2.37)	0.022*	0.225
	Coronal plane ROM	7.68 (1.93)	7.50 (2.48)	9.00 (2.22)	0.002*	0.334
	Maximum internal rotation angle	4.73 (4.04)	5.15 (4.31)	5.56 (4.00)	0.237	0.092
	Maximum external rotation angle	-5.27 (3.02)	-5.49 (3.30)	-4.41 (3.35)	0.917	0.052
	Transverse plane ROM	10.00 (3.27)	10.64 (4.05)	9.97 (3.81)	0.362	0.065
Trunk	Maximum Flexion angle	1.51 (8.23)	2.03 (8.89)	0.23 (8.27)	0.154	0.170
Kinematics (°)	Maximum Extension angle	-2.49 (7.90)	-2.52 (8.56)	-2.42 (8.12)	0.993	0.001
	Sagittal plane ROM	4.00 (1.47)	4.55 (1.92)	2.65 (0.90)	< 0.001*	0.516
	Maximum right lateral flexion angle	-4.30 (2.83)	-4.32 (3.20)	-3.72 (3.55)	0.392	.089
	Maximum left lateral flexion angle	6.53 (2.72)	6.67 (3.52)	7.01 (2.94)	0.708	0.033
	Coronal plane ROM	10.83 (3.08)	10.98 (2.14)	10.73 (2.37)	0.876	0.013
	Maximum internal rotation angle	4.69 (5.37)	5.30 (4.63)	4.13 (4.13)	0.300	0.113
	Maximum external rotation angle	-5.49 (3.91)	-4.93 (4.04)	-5.22 (2.88)	0.682	0.037
	Transverse plane ROM	10.18 (3.50)	10.23 (3.30)	9.34 (2.84)	0.250	0.129

SVA – Shank to Vertical Angle WA – Walker A

WB – Walker B

S-Shoe

ROM – Range of Motion

		WA	WB	S	p value	Effect Size
Ankle	Peak plantarflexion moment	-0.146 (0.12)	-0.173 (0.11)	-0.144 (0.10)	0.261	0.086
	Peak dorsiflexion moment	1.711 (1.35)	1.829 (1.29)	1.625 (1.07)	0.244	0.090
Knee	Peak extension moment after heel strike	-0.160 (0.13)	-0.219 (0.19)	-0.313 (0.22)	< 0.001*	0.461
	Peak flexion moment during mid stance phase	0.603 (0.39)	0.704 (0.45)	0.551 (0.38)	0.004*	0.306
	Peak extension moment during late stance phase	-0.397 (0.53)	-0.494 (0.47)	-0.279 (0.41)	< 0.001*	0.379
	First peak adduction moment	0.234 (0.16)	0.176 (0.12)	0.271 (0.18)	< 0.001*	0.449
	Second peak adduction moment	0.374 (0.56)	0.374 (0.48)	0.429 (0.45)	0.222	0.098
	First peak internal rotation moment	0.157 (0.09)	0.157 (0.10)	0.158 (0.10)	1.000	0.000
	Second peak internal rotation moment	0.040 (0.03)	0.030 (0.03)	0.037 (0.03)	0.264	0.085
Hip	Peak flexion moment	0.669 (0.41)	0.748 (0.47)	0.647 (0.42)	0.136	0.133
	Peak extension moment	-0.668 (0.39)	-0.650 (0.39)	-0.659 (0.39)	0.897	0.007
	First peak adduction moment	0.608 (0.32)	0.566 (0.33)	0.639 (0.35)	0.090	0.109
	Second peak adduction moment	0.602 (0.40)	0.580 (0.35)	0.660 (0.35)	0.041*	0.191
	Peak internal rotation moment	0.068 (0.07)	0.078 (0.08)	0.086 (0.08)	0.310	0.072
	Peak external rotation moment	-0.222 (0.12)	-0.202 (0.13)	-0.241 (0.15)	0.026*	0.216
WA - H	Valker A					

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446 Table 4: Mean (SD), main effects and effect sizes for kinetic variables (Nm/kg). Significance level p < 0.05. * Denotes significance

WA – Walker A

WB – Walker B

S - Shoe

			Mean Difference	p value	95% Confide	nce Intervals	
	S	WA	0.124	< 0.001*	0.074	0.174	
Gait Speed	S	WB	0.138	< 0.001*	0.081	0.194	
	WA	WB	-0.014	0.267	-0.012	0.039	
	Maximu	n tibial rec	line angle				
	S	WA	-2.206	0.014^{*}	-3.908	-0.504	
	S	WB	-3.987	$<\!\!0.001^*$	-6.024	-1.951	
	WA	WB	-1.781	0.012^{*}	-3.107	-0.455	
	Maximu	n tibial inc	lination angle				
	S	WA	2.759	0.001^{*}	1.303	4.215	
SVA	S	WB	1.712	0.026^{*}	0.230	3.195	
	WA	WB	-1.047	0.102	-2.328	0.234	
	Range						
	S	WA	4.966	0.001^{*}	2.362	7.570	
	S	WB	5.701	$< 0.001^{*}$	3.056	8.346	
	WA	WB	0.734	0.419	-1.149	2.618	
	Peak dur	ing early st	ance phase				
	S	WA	-11.448	0.304	-34.351	11.455	
	S	WB	-30.609	$< 0.001^{*}$	-44.168	-17.050	
hank Angular Valaaitu	WA	WB	-19.161	0.015^{*}	-34.106	-4.217	
nank Angular velocity	Peak during late stance phase						
	S	WA	-21.958	0.097	-48.368	4.452	
	S	WB	-50.195	$< 0.001^{*}$	-65.694	-34.696	
	WA	WB	-28.237	0.003^{*}	-45.117	-11.357	
	Plantar f	lexion angl	e during stance phase				
	S	WA	-9.615°	< 0.001*	7.879	11.351	
	S	WB	-9.809°	< 0.001*	8.238	11.380	
	WA	WB	-0.195°	0.724	-1.345	0.956	
Ankle Kinematics	Dorsi fle	xion angle	during stance phase				
	S	WA	6.018°	< 0.001*	-8.045	-3.991	
	S	WB	5.678°	< 0.001*	-7.367	-3.989	
	WA	WB	-0.339°	0.564	-1.564	0.886	
	Plantar f	exion angl	e during swing phase				

Table 3: Mean difference, post-hoc pairwise comparisons and 95% confidence intervals for ankle, knee, hip, pelvis & trunk kinematics. Significance level p<0.05.* Denotes significance

	S	WA	-17.807°	< 0.001*	14.165	21.449				
	S	WB	-18.476°	< 0.001*	15.064	-14.165				
	WA	WB	-0.669°	0.244	-1.844	0.506				
	Sagittal	plane angle a	t heel strike							
	S	WA	-2.617°	0.005^{*}	0.935	4.298				
	S	WB	-4.106°	< 0.001*	1.985	6.226				
	WA	WB	-1.489°	0.033*	-2.841	-0.137				
	Knee fle	Knee flexion angle during stance phase								
	S	WA	-2.384°	0.031*	0.251	4.516				
	S	WB	-5.099°	< 0.001*	2.891	7.306				
V	WA	WB	-2.715°	< 0.001*	-3.901	-1.530				
Knee Kinematics	Knee fle	Knee flexion angle during swing phase								
	S	WA	3.852°	0.014^{*}	-6.803	-0.901				
	S	WB	1.444°	0.246	-3.991	1.103				
	WA	WB	-2.408°	0.010^{*}	-4.161	-0.655				
	Knee abduction / valgus angle									
	S	WA	1.332°	0.003*	-2.130	-0.534				
	S	WB	1.289°	0.003*	-2.063	-0.515				
	WA	WB	-0.043°	0.905	-0.807	0.720				
	Hip sagi	ttal plane ran	ge of motion							
	S	WA	-1.567°	0.120	-0.461	3.594				
	S	WB	-2.059°	0.003*	0.835	3.283				
	WA	WB	-0.492°	0.505	-2.029	1.045				
	Hip adduction angle									
	S	WA	-3.044°	< 0.001*	1.688	4.400				
	S	WB	-2.545°	0.005^{*}	0.912	4.177				
Uin Vinomotios	WA	WB	0.500°	0.402	-0.735	1.734				
mp kinematics	Hip core	onal plane ran	ge of motion							
	S	WA	2.746°	< 0.001*	-3.795	-1.697				
	S	WB	2.850°	< 0.001*	-4.272	-1.429				
	WA	WB	0.105°	0.728	-0.526	0.735				
	Hip inte	rnal rotation a	angle							
	S	WA	-2.075°	0.030^{*}	0.229	3.922				
	S	WB	-2.726°	0.004^{*}	1.037	4.414				
	WA	WB	650°	0.389	-2.211	0.911				

	Hip tran	sverse plane	range of motion						
	S	WA	1.016°	0.070	-2.125	0.093			
	S	WB	1.214°	0.053	-2.445	0.017			
	WA	WB	0.198°	0.562	-0.514	0.911			
	Maximu	m Upwards	Pelvic Obliquity						
	S	ŴA	1.450°	0.014^{*}	-2.555	-0.345			
	S	WB	0.831°	0.141	-1.972	0.310			
DI ' 17' ('	WA	WB	-0.619°	0.158	-1.507	0.269			
Pelvis Kinematics	Pelvis C	oronal plane	range of motion						
	S	WA	1.319°	0.008^{*}	-2.235	-0.403			
	S	WB	1.501°	0.009^{*}	-2.561	-0.442			
	WA	WB	0.183°	0.578	-0.502	0.868			
	Trunk S	agittal plane	range of motion						
7 I I I 7 · · · ·	S	WA	-1.348°	0.005^{*}	0.518	2.178			
Trunk Kinematics	S	WB	-1.901°	0.006^{*}	0.687	3.116			
	WA	WB	-0.554°	0.115	-1.269	0.162			
	Peak knee extension after heel strike								
	S	WA	153 Nm/kg	< 0.001*	0.079	0.227			
	S	WB	094 Nm/kg	0.005^{*}	0.033	0.154			
	WA	WB	.059 Nm/kg	0.050^{*}	0.000	0.119			
	Peak flexion moment during mid-stance phase								
	S	WA	052 Nm/kg	0.240	-0.039	0.144			
	S	WB	153 Nm/kg	0.010^{*}	0.042	0.264			
Vara Vination	WA	WB	101 Nm/kg	0.006^{*}	-0.167	-0.034			
Knee Kinetics	Peak ext	Peak extension moment during late stance phase							
	S	WA	.118 Nm/kg	0.053	-0.238	0.002			
	S	WB	.215 Nm/kg	0.001^{*}	-0.333	-0.097			
	WA	WB	.096 Nm/kg	0.019^{*}	0.018	0.175			
	Peak add	duction mom	ent						
	S	WA	.037 Nm/kg	0.009^{*}	-0.063	-0.011			
	S	WB	.095 Nm/kg	$< 0.001^{*}$	-0.144	-0.046			
	WA	WB	.058 Nm/kg	0.015*	0.013	0.103			
	Peak add	duction mom	ent						
Hin Kinotios	S	WA	.058 Nm/kg	0.141	-0.138	0.022			
mp kinetics	S	WB	.080 Nm/kg	0.009^{*}	-0.136	-0.024			
	WA	WB	.022 Nm/kg	0.447	-0.038	0.082			

Peak ex	ternal rotation	n moment			
S	WA	019 Nm/kg	0.178	-0.010	0.047
S	WB	040 Nm/kg	0.022^{*}	0.006	0.073
WA	WB	021 Nm/kg	0.110	-0.047	0.005

SVA – Shank to Vertical Angle WA – Walker A WB – Walker B S - Shoe